



# Limiting amplitudes of fully nonlinear interfacial tides and solitons

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**Abstract.** A new two-fluid layer model consisting of forced rotation-modified Boussinesq equations is derived for studying tidally generated fully nonlinear, weakly nonhydrostatic dispersive interfacial waves. This set is a generalization of the Choi–Camassa equations, extended here with forcing terms and Coriolis effects. The forcing is represented by a horizontally oscillating sill, mimicking a barotropic tidal flow over topography. Solitons are generated by a disintegration of the interfacial tide. Because of strong nonlinearity, solitons may attain a limiting table-shaped form, in accordance with soliton theory. In addition, we use a quasi-linear version of the model (i.e. including barotropic advection but linear in the baroclinic fields) to investigate the role of the initial stages of the internal tide prior to its nonlinear disintegration. Numerical solutions reveal that the internal tide then reaches a limiting amplitude under increasing barotropic forcing. In the fully nonlinear regime, numerical experiments suggest that this limiting amplitude in the underlying internal tide extends to the nonlinear case in that internal solitons formed by a disintegration of the internal tide may not reach their table-shaped form with increased forcing, but appear limited well below that state.

ated by barotropic tidal flow over topography. As the internal tide steepens, it may split up into groups of internal solitons, which therefore appear at the tidal period.

For internal solitons as such, an archetypal model has been the Korteweg–de Vries (KdV) equation, which is based on the assumption of weak nonlinearity and weak nonhydrostaticity. The equation gives prediction for the relation between amplitude, width and phase speed of the solitons, as well as the shape itself. In the KdV equation there is, mathematically speaking, no limit to the amplitude that solitons may reach (although, of course, at some point the underlying assumption of weak nonlinearity would be violated). This behaviour changes fundamentally if a higher-order (i.e. cubic) nonlinear term is included, leading to the so-called extended KdV (eKdV) equation, as discussed in e.g. Helfrich and Melville (2006). This extended version produces qualitatively different solitons: their amplitude is limited (for a given configuration of layers) and they broaden as they reach their maximum amplitude, the so-called “table-top” solitons. This behaviour is confirmed by fully nonlinear soliton models, as derived by Choi and Camassa (1999) and Miyata (1985, 1988) (denoted as the MCC equations for brevity).

In this paper, we focus on another limiting factor, which comes into play even before solitons arise, namely in the internal tide itself. In a purely linear system, the amplitude of the internal tide increases linearly with the strength of the barotropic tidal flow. Here we study how this changes if one includes quasi-linear terms, i.e. retaining products of barotropic and baroclinic fields in the advective terms while still ignoring interactions of the baroclinic field with itself.

## 1 Introduction

Tidally generated internal solitons are a widespread phenomenon in the oceans and have been observed and studied for decades (see e.g. Apel et al., 2006). They are intrinsically linked to the internal tide, which itself is gener-

We demonstrate that a saturation in the amplitude of the internal tide occurs, and increasing the barotropic flow further does not produce a larger internal tide. As a consequence, when one includes the genuinely nonlinear effects, i.e. products of baroclinic terms, resulting solitons may stay well below their formal limiting amplitude, no matter how strong the forcing.

To study these effects we derived a set of fully nonlinear, weakly nonhydrostatic model equations, by extending the MCC equations with a barotropic tidal forcing over topography and with Coriolis effects, which have previously been shown to play a key role in soliton generation from internal tides (Gerkema and Zimmerman, 1995). To avoid having to deal with nonlinearities in the barotropic tide itself (which cannot be formally neglected in a fully nonlinear model), we mimic the interfacial wave generation, replacing a barotropic tidal flow over topography with a horizontally oscillating topography. (There is no exact equivalence between the two, but we demonstrate that, for the parameters used here, the difference remains small.) An alternative approach will also be discussed later.

The presence of a topography greatly complicates the subsequent handling of the equations, but we demonstrate that the set of equations can be obtained and can be cast in a form amenable to numerical solving.

An extension of the MCC theory with Coriolis effects (MCC- $f$ ) was already derived by Helfrich (2007), who investigated the decay and return of internal solitary waves with rotation. We focus on the novel aspect of studying the wave evolution and limiting amplitudes of fully nonlinear, weakly nonhydrostatic internal tides and solitons when forcing and rotational effects are added. We denote our extension of the MCC theory as forced-MCC- $f$  (or forced-MCC in the absence of rotation), for brevity.

The paper is organized as follows. We derive a new two-fluid layer model consisting of a set of forced rotation-modified Boussinesq equations in Sect. 2. We start with the basic equations and assumptions. Then, we scale equations (Sect. 2.1) and vertically integrate them over the layers (Sect. 2.2). Up to this point, the resulting equations are exact but do not form a closed set. The set is closed by making an expansion in a small parameter measuring the strength of nonhydrostaticity (Sect. 2.3). The resulting model turns out to be equivalent to the Choi–Camassa equations plus additional terms which represent the forcing and rotation effects. Prior to discussing the numerical experiments, we address in Sect. 3 some aspects related to the oscillating topography, the governing nondimensional parameters and the parameter values used for the runs. In Sect. 4 we investigate the factors limiting the growth of tidally generated solitons by first examining the generation of quasi-linear internal tides within the parameter space of this study. Next, in Sect. 5 we solve the full set of forced-MCC- $f$  and explore the conditions by which tide-generated fully nonlinear solitons may actually

attain a limiting amplitude. The main findings and conclusions are presented in Sect. 6.

The numerical methods and schemes are described in Appendix A. The full set of model equations as solved in the code is presented in Appendix B together with its (quasi)-linearized form. In Appendix C we compare, within the parameter space of this study, the case of an oscillating topography with the case of a tidal flow over a topography at rest.

## 2 Derivation of the forced-MCC- $f$ model

We start from the continuity and Euler equations and consider a two-fluid layer system (Fig. 1) with a jump in density across the interface and in which each layer is composed of a homogeneous, inviscid, and incompressible fluid; we apply the Boussinesq approximation. We also assume uniformity in one of the horizontal directions, taking  $\partial/\partial y = 0$ . Hence, the continuity and momentum equations read as

$$u_{i,x} + w_{i,z} = 0, \quad (1)$$

$$\bar{\rho} (u_{i,t} + u_i u_{i,x} + w_i u_{i,z} - f v_i) = -p_{i,x}, \quad (2)$$

$$v_{i,t} + u_i v_{i,x} + w_i v_{i,z} + f u_i = 0, \quad (3)$$

$$\bar{\rho} (w_{i,t} + u_i w_{i,x} + w_i w_{i,z}) = -p_{i,z} - \rho_i g, \quad (4)$$

where  $\rho_i$  is density,  $(u_i, v_i, w_i)$  are the velocity components in Cartesian coordinates,  $p_i$  is pressure,  $g$  the gravitational acceleration,  $f$  the Coriolis parameter ( $f = 2\Omega \sin \phi$ , at latitude  $\phi$ ) and  $\bar{\rho}$  the mean density. The subscript  $i = 1$  ( $i = 2$ ) refers to the upper (lower) layer, and a stable stratification,  $\rho_1 < \rho_2$ , is assumed.

Boundaries are defined at the surface, taken to be a rigid lid, which is located at  $z = H_1$ , and at the bottom, located at  $z = -H_2 + H(x, t)$ . The time dependence of the bottom will later be specified as a horizontal oscillation, mimicking a barotropic tidal flow over topography.

The kinematic boundary conditions at the surface and bottom read as

$$w_1 = 0 \text{ at } z = H_1, \quad (5)$$

$$w_2 = H_t + H_x u_2 \text{ at } z = -H_2 + H(x, t). \quad (6)$$

At the interface,  $z = Z(x, t)$ , the boundary conditions are given by the continuity of normal velocity and pressure:

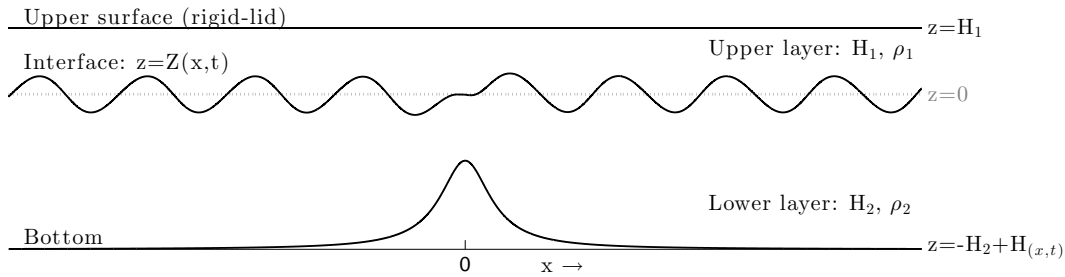
$$w_i = Z_t + u_i Z_x \text{ and } p_1 = p_2 \text{ at } z = Z. \quad (7)$$

For later convenience, we write pressure as the sum of hydrostatic and dynamic parts, the latter being denoted by primes:

$$p_i = \rho_i g H_1 - \rho_i g z + p'_i(t, x, z).$$

In the horizontal momentum equation, this amounts to replacing  $p_{i,x}$  with  $p'_{i,x}$ , whereas the vertical momentum equation (4) gives

$$\bar{\rho} (w_{i,t} + u_i w_{i,x} + w_i w_{i,z}) = -p'_{i,z}.$$



**Figure 1.** The two-fluid layer system for which the forced-MCC- $f$  equations are derived. The horizontal dashed grey line indicates the level  $z = 0$ , the level at which the interface resides at rest.

The second equation in (7), expressing continuity of pressure at the interface, now becomes

$$(p'_1 - p'_2)|_{z=Z} = (\rho_1 - \rho_2)gZ.$$

## 2.1 Scaling

The next step is to bring the equations into an appropriate dimensionless form for which we introduce the following scales. The scale for the undisturbed water depth is taken to be  $D$ , and the typical wavelength  $L$ . Crucially, we will assume waves to be long, i.e. nonhydrostatic effects to be weak. This will be expressed by the small parameter<sup>1</sup>,  $\delta = (D/L)^2 \ll 1$ .

Since we allow waves to have large amplitudes (i.e. to be strongly nonlinear), we may take horizontal current velocities to scale with  $c_0 = (g'D)^{1/2}$ , where  $g'$  is reduced gravity,  $g' = g(\rho_2 - \rho_1)/\bar{\rho}$ . (Notice that the exact linear long-wave phase speed for interfacial waves,  $c_p$ , is similar to  $c_0$ , but has  $H_1 H_2/D$  instead of  $D$  in the square root.) Thus,  $u$  and  $v$  will be scaled with  $c_0$ . As the interfacial displacement is allowed to be large, an appropriate scale of  $Z$  is  $D$ .

The typical scale of  $w$  now follows from the continuity equation as  $Dc_0/L$ . Finally, the scale of pressure follows from assuming a primary balance between the acceleration terms  $\bar{\rho} u_t$  and  $p_x$  in the horizontal momentum equation.

In summary, then, we can introduce the following dimensionless variables, indicated by asterisks,

$$\begin{aligned} x &= L x^*, \quad z = D z^*, \quad t = (L/c_0) t^*, \quad p'_i = (\bar{\rho} c_0^2) p'^*_i, \\ u_i &= c_0 u^*_i, \quad v_i = c_0 v^*_i, \quad w_i = (D/L) c_0 w^*_i. \end{aligned} \quad (8)$$

With these scales, the dimensionless continuity and Euler equations yield (for convenience, we drop the asterisks right away)

$$u_{i,x} + w_{i,z} = 0, \quad (9)$$

$$u_{i,t} + u_i u_{i,x} + w_i u_{i,z} - \mu v_i = -p'_{i,x}, \quad (10)$$

$$v_{i,t} + u_i v_{i,x} + w_i v_{i,z} + \mu u_i = 0, \quad (11)$$

<sup>1</sup>In Choi and Camassa (1999) a small parameter  $\epsilon$  was used instead, which relates to ours as  $\delta = \epsilon^2$ .

$$\delta (w_{i,t} + u_i w_{i,x} + w_i w_{i,z}) = -p'_{i,z}. \quad (12)$$

Here  $\mu$  is the scaled Coriolis parameter,  $\mu = fL/c_0$ . Furthermore, we introduce the dimensionless quantities  $\zeta$ ,  $h_i$ , and  $h$  via  $(Z, H_1, H_2, H) = D(\zeta, h_1, h_2, h)$ , so that the scaled form of the boundary conditions is

$$w_1 = 0 \text{ at } z = h_1, \quad (13)$$

$$w_i = \zeta_t + u_i \zeta_x \text{ at } z = \zeta(x, t), \quad (14)$$

$$p'_2 - p'_1 = \zeta \text{ at } z = \zeta(x, t), \quad (15)$$

$$w_2 = h_t + u_2 h_x \text{ at } z = -h_2 + h(x, t). \quad (16)$$

The goal is now to derive a reduced set of equations from Eqs. (9) to (12), in which the boundary conditions (13)–(16) are incorporated by vertical integration, exploiting the smallness of the parameter  $\delta$ . The procedure is identical to that of Choi and Camassa (1999), but with the additional complications of the Coriolis force, topography, and tidal forcing.

## 2.2 Vertically integrated equations

We vertically integrate the equations over the upper and lower layers and expand them to the orders  $\delta^0$  and  $\delta^1$  to obtain a closed set for the weakly nonhydrostatic equations, following Choi and Camassa (1999). The layer mean  $\bar{f}_1$  of a function  $f_1(x, z, t)$  for the upper layer is defined as

$$\bar{f}_1(x, t) = \frac{1}{\eta_1} \int_{\zeta}^{h_1} dz f_1(x, z, t), \quad \eta_1 = h_1 - \zeta, \quad (17)$$

and for the lower layer as

$$\bar{f}_2(x, t) = \frac{1}{\eta_2} \int_{-h_2+h}^{\zeta} dz f_2(x, z, t), \quad \eta_2 = h_2 - h + \zeta, \quad (18)$$

where  $\eta_i$  represents the thickness of the layer (depending on the interfacial displacement  $\zeta$ ). Notice that the boundaries of the integral depend on time and space ( $x$ ) via the interfacial movement  $\zeta(t, x)$ , but also, for the lower layer, via the horizontally oscillating topography<sup>2</sup>,  $h(t, x)$ . Before

<sup>2</sup>For this reason we need to apply the Leibniz integral rule below with respect to  $x$  and  $t$ .

proceeding, nonlinear terms in the horizontal momentum equations (10) and (11) are rewritten as  $(u_i^2)_x + (w_i u_i)_z$  and  $(u_i v_i)_x + (w_i v_i)_z$ , respectively, to facilitate the procedure.

After integration of Eqs. (9)–(11) for  $i = 1$  and applying the boundary conditions (13)–(15), we obtain the layer-mean equations for the upper layer:

$$\eta_{1,t} + (\eta_1 \bar{u}_1)_x = 0, \quad (19)$$

$$(\eta_1 \bar{u}_1)_t + (\eta_1 \bar{u}_1 \bar{u}_1)_x - \mu \eta_1 \bar{v}_1 = -\eta_1 \bar{p}'_{1,x}, \quad (20)$$

$$(\eta_1 \bar{v}_1)_t + (\eta_1 \bar{u}_1 \bar{v}_1)_x + \mu \eta_1 \bar{u}_1 = 0. \quad (21)$$

For the lower layer one proceeds similarly, except that now both boundaries are variable. Applying the boundary conditions (14)–(16), vertical integration of Eqs. (9)–(11) for  $i = 2$  yields

$$\eta_{2,t} + (\eta_2 \bar{u}_2)_x = 0, \quad (22)$$

$$(\eta_2 \bar{u}_2)_t + (\eta_2 \bar{u}_2 \bar{u}_2)_x - \mu \eta_2 \bar{v}_2 = -\eta_2 \bar{p}'_{2,x}, \quad (23)$$

$$(\eta_2 \bar{v}_2)_t + (\eta_2 \bar{u}_2 \bar{v}_2)_x + \mu \eta_2 \bar{u}_2 = 0. \quad (24)$$

### 2.3 Expansion in $\delta$

The six integrated Eqs. (19)–(24) derived so far are exact but do not form a closed set. The variables  $\eta_1, \eta_2$  and  $\zeta$  count as one unknown, but we also have  $\bar{u}_i, \bar{v}_i, \bar{p}'_{i,x}, \bar{u}_i \bar{u}_i$  and  $\bar{u}_i \bar{v}_i$ , giving 11 unknowns for 6 equations. To obtain a closed set, the last two expressions will be cast in terms of  $\bar{u}_i$  and  $\bar{v}_i$  by using the vertical momentum equation, expanded in terms of the small parameter  $\delta$ . Furthermore, continuity of pressure at the interface is used to connect the pressure in the lower and upper layers (i.e.  $\bar{p}'_{1,x}$  and  $\bar{p}'_{2,x}$ ). All in all, the six equations are thus modified to contain only six unknowns. With this aim, we make a formal expansion of the unknowns for the lowest ( $\delta^0$ ) and next ( $\delta$ ) orders, as, for example,

$$\bar{f}_i = \bar{f}_i^{(0)} + \delta \bar{f}_i^{(1)} + \dots$$

At the lowest order ( $\delta^0$ ),  $p'^{(0)}$ , the dynamics is hydrostatic. At the next order ( $\delta$ ),  $p'^{(1)}$  brings weakly nonhydrostatic effects into the system.

#### 2.3.1 Lowest order

At lowest order, the vertical momentum equation (12) reduces to  $\partial p_i^{(0)} / \partial z = 0$  as terms of order  $\delta$  are neglected; therefore, (perturbation) pressure is vertically constant in each layer. For convenience, we introduce  $P = p_2^{(0)}$ , being a function of  $t$  and  $x$ . It then follows from continuity of pressure at the interface that  $p_1^{(0)} = P - \zeta$ . Thus, to this order of approximation,

$$\bar{p}'_{1,x} = P_x - \zeta_x + O(\delta), \quad (25)$$

and, for the lower layer,

$$\bar{p}'_{2,x} = P_x + O(\delta). \quad (26)$$

Given the  $z$  independence of pressure and returning to the original horizontal momentum equations, it is now natural to assume that the horizontal velocities, too, are independent of  $z$  within each layer:

$$\bar{u}_i \bar{u}_i = \bar{u}_i^2 + O(\delta), \quad \bar{u}_i \bar{v}_i = \bar{u}_i \bar{v}_i + O(\delta).$$

At lowest order, then, the set of integrated equations is closed; together with the (exact) integrated continuity equations (19) and (22), we have the momentum equations in terms of the six variables  $\bar{u}_i, \bar{v}_i, \zeta$  and  $P$ :

$$(\eta_1 \bar{u}_1)_t + (\eta_1 \bar{u}_1^2)_x - \mu \eta_1 \bar{v}_1 = -\eta_1 (P_x - \zeta_x) + O(\delta), \quad (27)$$

$$(\eta_2 \bar{u}_2)_t + (\eta_2 \bar{u}_2^2)_x - \mu \eta_2 \bar{v}_2 = -\eta_2 P_x + O(\delta), \quad (28)$$

$$(\eta_1 \bar{v}_1)_t + (\eta_1 \bar{u}_1 \bar{v}_1)_x + \mu \eta_1 \bar{u}_1 = O(\delta), \quad (29)$$

$$(\eta_2 \bar{v}_2)_t + (\eta_2 \bar{u}_2 \bar{v}_2)_x + \mu \eta_2 \bar{u}_2 = O(\delta). \quad (30)$$

Recall that  $\eta_{1,2}$  can be expressed in terms of  $\zeta$  and thus involve just one unknown.

#### 2.3.2 Next order

At order  $\delta$ , the procedure is to close the set of six vertically integrated equations by deriving expressions for the horizontal pressure gradients  $\bar{p}'_{i,x}$  as well as for the contributions of  $\bar{u}_i \bar{u}_i$  and  $\bar{u}_i \bar{v}_i$  in the nonlinear terms. The latter problem is particularly simple. At order  $\delta$ , the products contain one lowest-order field, which is independent of  $z$  (e.g.  $u_i^{(0)} = \bar{u}_i^{(0)}$ ); hence,

$$\begin{aligned} \bar{u}_i \bar{u}_i &= \frac{1}{\eta_i} \int dz u_i^2 = \frac{1}{\eta_i} \int dz \left( u_i^{(0)2} + 2\delta u_i^{(0)} u_i^{(1)} + \dots \right) \\ &= \bar{u}_i^{(0)2} + 2\delta \bar{u}_i^{(0)} \bar{u}_i^{(1)} + \dots \\ &= \bar{u}_i^2 + O(\delta^2), \end{aligned}$$

so that

$$\bar{u}_i \bar{u}_i = \bar{u}_i^2 + O(\delta^2), \quad \bar{u}_i \bar{v}_i = \bar{u}_i \bar{v}_i + O(\delta^2).$$

This allows us to write the horizontal momentum equations as

$$(\eta_1 \bar{u}_1)_t + (\eta_1 \bar{u}_1^2)_x - \mu \eta_1 \bar{v}_1 = -\eta_1 (\bar{p}_1^{(0)} + \delta \bar{p}_1^{(1)})_x + O(\delta^2), \quad (31)$$

$$(\eta_2 \bar{u}_2)_t + (\eta_2 \bar{u}_2^2)_x - \mu \eta_2 \bar{v}_2 = -\eta_2 (\bar{p}_2^{(0)} + \delta \bar{p}_2^{(1)})_x + O(\delta^2), \quad (32)$$

$$(\eta_1 \bar{v}_1)_t + (\eta_1 \bar{u}_1 \bar{v}_1)_x + \mu \eta_1 \bar{u}_1 = O(\delta^2), \quad (33)$$

$$(\eta_2 \bar{v}_2)_t + (\eta_2 \bar{u}_2 \bar{v}_2)_x + \mu \eta_2 \bar{u}_2 = O(\delta^2). \quad (34)$$

The remaining problem is to find an expression for  $\bar{p}_i^{(1)}$ . At order  $\delta$ , Eq. (12) reads, in terms of the lowest-order vertical velocities,

$$w_i^{(0)}{}_t + u_i^{(0)} w_i^{(0)}{}_x + w_i^{(0)} w_i^{(0)}{}_z = -p_i^{(1)}{}_z. \quad (35)$$

By vertically integrating the continuity equation (9), we obtain an expression for  $w_i^{(0)}$ :

$$w_i^{(0)} = -z \bar{u}_{i,x}^{(0)} + c_i(t, x),$$

where  $c_i$  are “constants” of integration which are determined by using the boundary conditions at the surface (13) and bottom (16). Thus,  $w_i^{(0)}$  for the upper and lower layers become, respectively,

$$w_1^{(0)} = (h_1 - z) \bar{u}_{1,x}^{(0)}, \quad (36)$$

$$w_2^{(0)} = (h - h_2 - z) \bar{u}_{2,x}^{(0)} + D_2 h, \quad (37)$$

where the operator  $D_i$  is defined as  $\partial/\partial t + \bar{u}_i^{(0)}\partial/\partial x$ . Substituting  $w_1^{(0)}$  from Eq. (36) and  $w_2^{(0)}$  from Eq. (37) into Eq. (35), and vertically integrating the result, we get an expression for  $p_1^{(1)}$  and  $p_2^{(1)}$ . Taking their derivative with respect to  $x$  and their mean over each layer, we finally obtain an expression for  $\overline{p_i^{(1)}}_x$  at order  $\delta$ . Including the lowest-order terms (25) and (26), this allows us to write the horizontal pressure gradient for the upper layer,

$$\begin{aligned} \overline{p'_{1,x}} &= \overline{p'_{1,x}}^{(0)} + \delta \overline{p'_{1,x}}^{(1)} + O(\delta^2) \\ &= P_x - \zeta_x - \delta \left[ \frac{1}{3\eta_1} (\eta_1^3 G_1)_x \right] + O(\delta^2), \end{aligned} \quad (38)$$

and, for the lower layer,

$$\begin{aligned} \overline{p'_{2,x}} &= \overline{p'_{2,x}}^{(0)} + \delta \overline{p'_{2,x}}^{(1)} + O(\delta^2) \\ &= P_x - \delta \left[ \frac{1}{3\eta_2} (\eta_2^3 G_2)_x + \frac{1}{2} \eta_2 G_2 h_x \right. \\ &\quad \left. - \frac{\eta_2}{2} (D_2^2 h)_x - \zeta_x D_2^2 h \right] + O(\delta^2), \end{aligned} \quad (39)$$

where we introduced for simplicity the term  $G_i$  (as in Choi and Camassa, 1999),

$$G_i = \bar{u}_{i,x}^{(0)} + \bar{u}_i^{(0)} \bar{u}_{i,xx}^{(0)} - (\bar{u}_{i,x}^{(0)})^2. \quad (40)$$

With this, the horizontal momentum equations (31) and (32) become

$$\begin{aligned} &(\eta_1 \bar{u}_1)_t + (\eta_1 \bar{u}_1^2)_x - \mu \eta_1 \bar{v}_1 \\ &= -\eta_1 \left\{ P_x - \zeta_x - \delta \left[ \frac{1}{3\eta_1} (\eta_1^3 G_1)_x \right] \right\} + O(\delta^2) \\ &(\eta_2 \bar{u}_2)_t + (\eta_2 \bar{u}_2^2)_x - \mu \eta_2 \bar{v}_2 \\ &= -\eta_2 \left\{ P_x - \delta \left[ \frac{1}{3\eta_2} (\eta_2^3 G_2)_x + \frac{1}{2} \eta_2 G_2 h_x \right. \right. \\ &\quad \left. \left. - \frac{\eta_2}{2} (D_2^2 h)_x - \zeta_x D_2^2 h \right] \right\} + O(\delta^2). \end{aligned} \quad (41)$$

We have thus obtained a closed set of six dimensionless equations, namely the exact continuity equations (19) and (22), the horizontal momentum equations (41) and (42), as well as (33) and (34); the last four equations involve the weakly nonhydrostatic assumption. The six unknowns are  $\bar{u}_1$ ,  $\bar{u}_2$ ,  $\bar{v}_1$ ,  $\bar{v}_2$ ,  $P$ , and (via  $\eta_{1,2}$ )  $\zeta$ . Without interfacial forcing and Earth's rotation, our set of equations correctly reduces to that of Choi and Camassa (1999). We further specify the

model by prescribing the oscillating topography, i.e. the forcing to the system, with

$$h = h(X) \text{ where } X(x, t) = x - U_0 \cos t, \quad (43)$$

and  $U_0$  is an arbitrary positive constant.

We combine the continuity equations (19) and (22) into

$$(\eta_1 + \eta_2)_t + (\eta_1 \bar{u}_1 + \eta_2 \bar{u}_2)_x = 0. \quad (44)$$

Given that  $\eta_1 + \eta_2 = h_1 + h_2 - h$ , with the two-fluid system depth  $h_1 + h_2 = 1$ , this leads to

$$-h_t + (\eta_1 \bar{u}_1 + \eta_2 \bar{u}_2)_x = 0. \quad (45)$$

If we now substitute the time derivative of the oscillating topography (43), we have

$$(\eta_1 \bar{u}_1 + \eta_2 \bar{u}_2)_x = U h_x, \quad (46)$$

with

$$U = U_0 \sin t, \quad (47)$$

which is the velocity of the oscillating topography with amplitude  $U_0$ , mimicking a barotropic tidal flow. However, the two are not exactly equivalent, since the transformation from one frame of reference to the other involves an acceleration, and is therefore not Galilean. We discuss this aspect further in Appendix C.

Equation (46) can be then integrated in  $x$ :

$$\eta_1 \bar{u}_1 + \eta_2 \bar{u}_2 = U h + C(t). \quad (48)$$

Far from the sill (i.e.  $h \rightarrow 0$  for  $x \rightarrow \pm\infty$ ), we impose the flow to be purely baroclinic, so that the left-hand side must be zero, and hence it follows that  $C(t) = 0$ . Notice that the right-hand side is prescribed via the forcing and thus is a known quantity. It allows us to express  $\bar{u}_2$  in terms of  $\bar{u}_1$ .

We can thus combine the horizontal momentum equations (41) and (42), eliminating  $P$ ,

$$\begin{aligned} \bar{u}_{1,t} + \bar{u}_1 \bar{u}_{1,x} + \mu \bar{v}_1 &= \zeta_x + \frac{1}{(1-h)} \\ &\quad \left( (U h)_t + (\eta_1 \bar{u}_1^2 + \eta_2 \bar{u}_2^2)_x \right. \\ &\quad \left. - \mu (\eta_1 \bar{v}_1 + \eta_2 \bar{v}_2) - \eta_1 \zeta_x \right) \\ &\quad + \delta \left( 1 - \frac{\eta_1}{(1-h)} \right) \left[ \eta_1 G_1 \eta_{1,x} + \frac{\eta_1^2}{3} G_{1,x} \right] \\ &\quad + \frac{\delta \eta_2}{(1-h)} \left[ -\eta_2 G_2 \zeta_x - \frac{\eta_2^2}{3} G_{2,x} \right. \\ &\quad \left. + \frac{\eta_2 G_2}{2} h_x + \frac{\eta_2}{2} (D_2^2 h)_x + \zeta_x D_2^2 h \right] + O(\delta^2) \end{aligned} \quad (49)$$

$$\bar{u}_2 = \frac{U h - \eta_1 \bar{u}_1}{\eta_2}, \quad (50)$$

$$\bar{v}_{1,t} + \bar{u}_1 \bar{v}_{1,x} + \mu \bar{u}_1 = O(\delta^2), \quad (51)$$

$$\bar{v}_{2,t} + \bar{u}_2 \bar{v}_{2,x} + \mu \bar{u}_2 = O(\delta^2), \quad (52)$$

$$\zeta_t - (h_1 - \zeta) \bar{u}_{1,x} + \bar{u}_1 \zeta_x = 0, \quad (53)$$

where the  $\bar{v}_i$ -horizontal momentum equations (51) and (52) have been further simplified from Eqs. (33) and (34) by using the continuity equations (19) and (22). Equation (19) has now been expressed in terms of  $\zeta$  for convenience. The other continuity equation (22) is no longer included since it is already implicitly present via Eq. (50).

All in all, we now have five equations for five unknowns ( $\bar{u}_1$ ,  $\bar{u}_2$ ,  $\bar{v}_1$ ,  $\bar{v}_2$  and  $\zeta$ ). The numerical methods and schemes used to solve the model are described in Appendix A. The actual form of the model equations as used in the numerical code is presented in Appendix B. In Appendix C we compare, within the parameter space of this study, the case of an oscillating topography with the case of a tidal flow over a topography at rest.

Before concluding this section, it is worthwhile noting an alternative approach. Given the assumption of a rigid lid, one could have also taken  $U = 0$  in Eq. (48), the topographic motion set to zero, and then prescribed an external barotropic flux via  $C(t)$ . Imposing a barotropic flux in this manner does not allow for spatial variations of that flux, as would occur with a free surface, for which an additional dynamical equation would be required to solve the barotropic mode. Specification of  $C(t)$  is common in fully nonlinear models of this type as, for example, in Lamb (1994) and Vlasenko et al. (2005). However, the choice of an oscillating topography has also proven to be of use in the study of strongly nonlinear interfacial waves. For instance, Grue (2015) recently confirmed findings on the onset of wave train formation observed in experimental measurements by Maxworthy (1979) with a three-dimensional two-layer, fully dispersive and strongly nonlinear interfacial wave model with a time-varying bottom topography.

### 3 Numerical experiments: preliminary remarks

Whilst not designed to represent a specific region of the world oceans, we aim to investigate in a general manner the conditions by which tidally generated solitons may evolve and, eventually, develop limiting amplitudes in ocean-like scenarios. It is then desirable that leading solitons can propagate towards a mature stage before overtaking preceding internal tides; otherwise, although these are form-preserving features, the tracking of their wave properties becomes cumbersome. For this reason, the parameters that we describe in the following were selected to highlight the qualitative features of these nonlinear processes for a broad range of (mimicked) tidal forcing strengths.

Although the model is solved and discussed in nondimensional form, we also present the parameter values in dimensional form to put them in an oceanographic context.

#### 3.1 The oscillating topography and the hydraulic state: the Froude number

We define the (dimensional) topography analytically following

$$H(X) = \frac{H_T}{1 + (x/H_L)^2}, \quad (54)$$

with  $x$  being the grid positions in space, and  $H_T$  and  $H_L$  being the dimensional parameters which set the height and width of a symmetric sill, respectively. In this manner we ensure perfectly smooth second and third derivatives of the dimensionless topography  $h(X)$  in the model equations.

At this point it is worthwhile recalling that the oscillation of the topography is introduced in dimensionless form as  $h = h(X)$  with  $X(x, t) = x - U_0 \cos t$ , where  $U_0$  prescribes the strength (velocity amplitude) of the oscillating topography via  $U = U_0 \sin(t)$ , the mimicked barotropic tidal flow (see Eqs. 43–47). By increasing  $U_0$  we enhance the forcing via  $U$ , which in dimensional form we introduce, respectively, as  $U_0 = c_0 U_0$  and  $U = c_0 U$ .

The topographic obstacle (ridge, sill, etc.) is always centered on the  $x$  axis and the length of the  $x$  domain is chosen to be large enough to prevent waves from reaching the boundaries. In all experiments, the topography starts moving to the left at  $t = 0$ ; we start with a system at rest, i.e.  $U = \bar{u}_1 = \bar{u}_2 = 0$  at  $t = 0$ . The waves are generated near the origin; on the negative (positive)  $x$  axis, waves travel to the left (right). Because the forcing starts asymmetrically, it is expected that wave packets in the front appear rather differently when comparing both sides (negative vs. positive  $x$  domain). These fronts are the transients, which are influenced by the way the experiment is started. A steady solution at both sides of the  $x$  axis is reached after several tidal periods have passed. In this regard, and to avoid transient effects generated at the start of each run, wave properties have been tracked systematically for the third leftward-propagating interfacial wave counting from the front and after nine tidal periods of forcing.

To characterize the hydraulic state, we use the Froude number calculated as

$$Fr = \frac{U_0}{c_p}, \quad (55)$$

where the amplitude of the mimicked tidal flow,  $U_0$ , is compared to the linear long-wave phase speed for interfacial waves,  $c_p$ . The strength of  $U_0$  leads to three different regimes of interfacial wave generation (see e.g. Vlasenko et al., 2005; Da Silva et al., 2015). Accordingly, the hydraulic regime is denoted, hereafter, as subcritical when  $Fr \ll 1$ , critical when  $Fr \approx 1$ , and supercritical when  $Fr > 1$ . To account for the varying strength of the tidal forcing within a tidal cycle, we introduce the instantaneous Froude number, defined as  $Fr' = U/c_p$ .

Importantly, we also use the Froude number in Appendix C to discuss the applicability of our “non-inertial” frame of reference, the oscillating topography, to the ocean case, where the topography is at rest. To this aim we compare the generation of interfacial waves from the (quasi-)linear forced-MCC equations with that from the (quasi-)linear version of the weakly nonlinear model derived in Gerkema (1996), which works with actual tidal motion. Recall that in the quasi-linear case, barotropic advection is retained but baroclinic interactions are neglected. The equations are then still linear with regard to the baroclinic fields, but the coefficients become time-dependent due to barotropic factors (which are prescribed), so that higher harmonics will be generated when the forcing is increased. For clarification, the (quasi-)linearization of the forced-MCC- $f$  equations is presented in Appendix B.

Results from this model comparison confirm a near equivalence between both models within the parameter framework of study, which we restrict to  $0 < Fr < 1.6$ . This encourages us to discuss our numerical results, henceforth referring to the strength of the topographic oscillation,  $U_0$ , as the strength of the tidal flow.

### 3.2 Parameter values

We adopt a two-layer system where the total water depth,  $D$ , is set to 100 m, with the upper layer always being thinner than the lower layer ( $H_1 < H_2$ ). The horizontal oscillation of the moving topography is always of semidiurnal frequency. Although the height of the topography varies between runs, its horizontal scale is kept constant and about 20 km ( $H_L = 10$  km in Eq. 54). Regarding reduced gravity,  $g'$  typically ranges from  $0.007 \text{ m s}^{-2}$  in the Celtic Sea (Gerkema, 1996) to  $0.027 \text{ m s}^{-2}$  over the Oregon continental shelf (Stanton and Ostrovsky, 1998); we use this range accordingly.

In Table 1 the varying parameters are listed. They vary between runs as indicated in bold fonts, one at a time. The theoretical amplitude of the “table-top” soliton predicted from Eq. (3.68) in Choi and Camassa (1999), and beyond which no solitary wave solution exists, is also indicated.

In Sect. 4, runs A1, A2 and A3 illustrate the effect of varying stratification via the reduced gravity,  $g'$ . Runs A1, B1 and B2 illustrate the effect of varying the topography ratio,  $\varphi_T = H_T/D$ , the height of the topography relative to the total water depth. Finally, runs A1, C1 and C2 illustrate the effect of varying the two-fluid layer thickness ratio,  $\gamma = H_1/H_2$ . Based on the results from the above analyses, we will argue later why in Sect. 5 we focus on a highly stratified regime ( $g' = 0.03 \text{ m s}^{-2}$ ) for the study of fully nonlinear waves.

For convenience, wave properties are scaled as follows. The interfacial displacement,  $Z$ , the internal tide amplitude,  $A$ , and the soliton amplitude,  $A_s$ , are scaled to the thickness of the upper layer,  $H_1$ . The soliton phase speed,  $c_s$ , is scaled to the phase speed of linear long-wave interfacial

waves,  $c_p$ . Horizontal distances along the  $x$ -direction and the soliton width,  $L_s$ , are scaled to the wavelength of linear long-wave interfacial waves,  $L_p$ . Finally, we use the scaled Coriolis parameter,  $\mu_p$ , which relates to  $\mu$  in Sect. 2.1, following  $\mu_p = \mu/(2\pi)$ .

### 4 Numerical experiments: quasi-linear internal tides

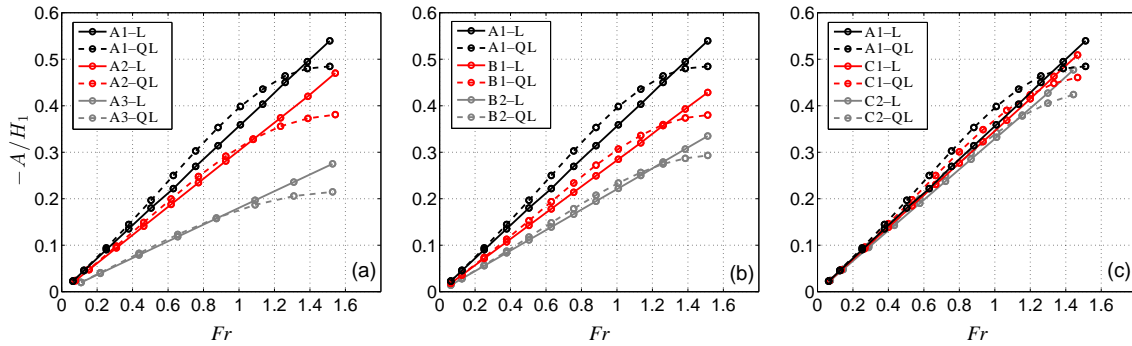
Tide-generated solitons emerge from nonlinear disintegration of the underlying internal tides and may be, therefore, naturally subjected to the properties of the latter. For this reason, we find it insightful to investigate first the properties of the underlying internal tides, prior to their nonlinear disintegration, within the parameter space of this study.

As described in Sect. 3, the quasi-linear case includes advective terms from the interactions between the barotropic and baroclinic flows, while interactions between baroclinic fields, the genuinely nonlinear terms, are still absent. Therefore, higher harmonics are naturally generated when the forcing is increased. The linear case, where all advective terms are absent, is included here to assess potential departures from the quasi-linear case.

Accordingly, Fig. 2 presents the internal tide response to the strength of the tidal forcing for runs A1 to C2 (see Table 1). The minimum forcing strength for all cases is  $U_0 = 5 \text{ cm s}^{-1}$ . In subsequent data points, the increase in  $U_0$  is  $10 \text{ cm s}^{-1}$  from  $U_0 = 10 \text{ cm s}^{-1}$  and onwards, reaching up to  $Fr \sim 1.5$ .

In the purely linear experiments, the amplitude of the internal tide increases linearly with the barotropic tidal flow strength. However, the quasi-linear internal tide exhibits a limiting amplitude in all runs, when the tidal forcing increases well above  $Fr = 1$ , a feature that seems to have passed unnoticed in earlier studies. For weak forcing ( $Fr \ll 1$ ), the amplitude of the quasi-linear internal tides approaches the linear case; the advective terms then become very small. This pattern indicates that the decisive factor in the amplitude saturation of quasi-linear internal tides lies in the barotropic advection, which is absent in the linear case.

Regarding the comparison between runs with different parameters, we find the following. In Fig. 2a, the increase in stratification causes an earlier deviation between the amplitude growth of the quasi-linear and linear cases, hence occurring at a lower Froude number for runs with a higher stratification (cf. runs A1, A2 and A3). The same effect is observed in Fig. 2b when the height of the topography is increased. The higher the topography, the earlier a deviation from the linear case appears in the Froude number space (cf. runs A1, B1 and B2). Finally, no significant differences emerge regarding the rise of the quasi-linear departure in Fig. 2c, where the thickness of the upper layer varies (cf. runs A1, C1 and C2). These results indicate that the deviation from the linear case arises for lower Froude numbers if either the strength of the stratification or the height of the topography increases.



**Figure 2.** Amplitude of the linear,  $L$ , and quasi-linear,  $QL$ , internal tide scaled to the thickness of the upper layer vs. the Froude number. Varying parameters between panels are **(a)** the strength of stratification,  $g'$  (runs A1, A2 and A3); **(b)** the topography ratio,  $\varphi_T$  (runs A1, B1 and B2); and **(c)** the two-fluid layer thickness ratio,  $\gamma$  (runs A1, C1 and C2). The run time is nine tidal periods. See Table 1 for further details.

**Table 1.** Summary of runs. Varying parameters are the reduced gravity,  $g'$  ( $\text{m s}^{-2}$ ), the topography ratio,  $\varphi_T$ , and the two-fluid layer thickness ratio,  $\gamma$ . The theoretical maximum amplitude,  $A_m$ , as predicted from Eq. (3.68) in Choi and Camassa (1999), is also indicated.

Run	$g'$ (in $\text{m s}^{-2}$ )	$\varphi_T = H_T/D$	$\gamma = H_1/H_2$	$-A_m/H_1$	$H_1, H_2$ (in m)	$\rho_1, \rho_2$ ( $\text{kg m}^{-3}$ )
A1	<b>0.03</b>	0.4	0.43	0.67	30, 70	1022, 1025.15
A2	<b>0.02</b>	0.4	0.43	0.67	30, 70	1023.05, 1025.15
A3	<b>0.01</b>	0.4	0.43	0.67	30, 70	1024.1, 1025.15
B1	0.03	<b>0.35</b>	0.43	0.67	30, 70	1022, 1025.15
B2	0.03	<b>0.3</b>	0.43	0.67	30, 70	1022, 1025.15
C1	0.03	0.4	<b>0.33</b>	1	25, 75	1022, 1025.15
C2	0.03	0.4	<b>0.25</b>	1.5	20, 80	1022, 1025.15

Although not shown, it is worth mentioning that the wavelength of the quasi-linear tides does not deviate from the linear case in any of the settings of study and is independent of the strength of the tidal forcing (and hence of the Froude number) and of the height of the topography. However, as predicted from linear theory for interfacial waves, an increase in  $g'$  or  $H_1$  (with  $H_1 < H_2$  and  $D$  being constant) generates longer internal tides.

The amplitude saturation described above is further illustrated in Fig. 3 for run A1, where snapshots of leftward-propagating quasi-linear internal tides are shown for various forcing strengths (see legend). This spatial view shows how the increase in the forcing transforms the wave from a sinusoidal to an asymmetric shape, indicative of the presence of higher harmonics, while the amplitude becomes saturated.

These findings raise the question as to whether solitons emerging from a disintegration of the initially quasi-linear internal tides may be subjected to saturation before they reach a limiting “table-top” shape. We examine this question in the next section by focussing on runs A1, B1 and C1, varying the height of the topography and the thickness of the upper layer while preserving a high stratification. The latter allows us to investigate the broadest range of interfacial wave amplitudes, as suggested by Fig. 2a.

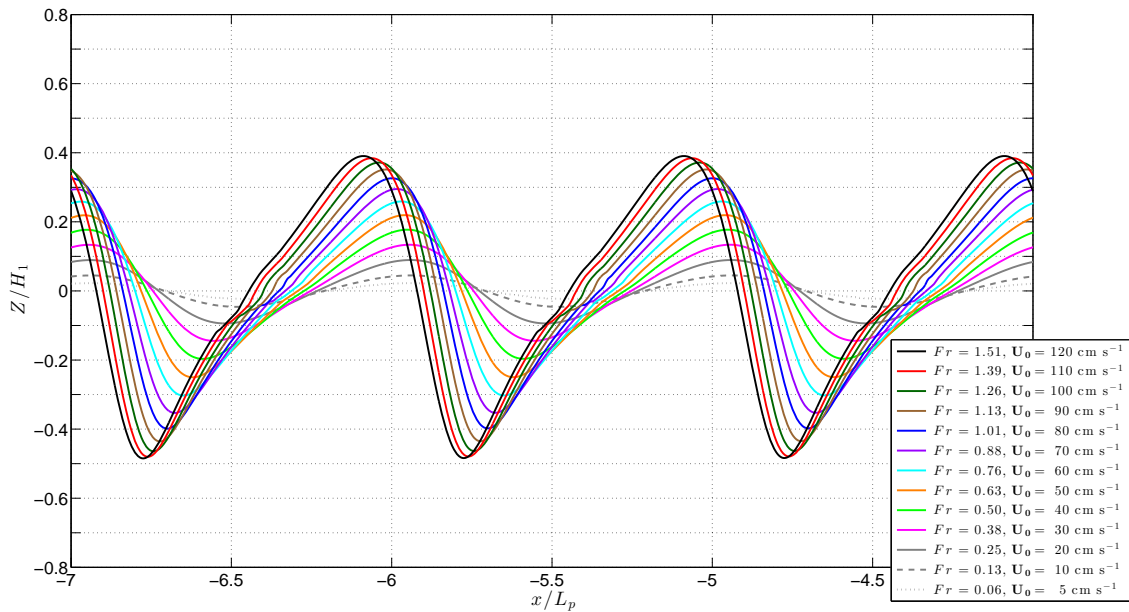
## 5 Numerical experiments: fully nonlinear internal tides and solitons

In this section we investigate the conditions by which tidally generated fully nonlinear solitons may attain a limiting amplitude. Special attention is devoted to factors conditioning the growth of fully nonlinear waves as “table-top” solitons. The main question to address is whether the amplitudes of tidally generated solitons may be subjected to limiting amplitudes of the underlying quasi-linear internal tides, as we hypothesized in the previous section, thus qualifying predictions from classical eKdV and MCC theories.

### 5.1 Tide-generated “table-top” solitons: run A1

In Fig. 4a a spatial overview of leftward-propagating internal tides and solitons is shown after nine tidal periods of run time. The tidal forcing is fairly strong and this leads to the generation of “table-top” solitons in a supercritical regime ( $Fr = 1.13$ ,  $U_0 = 90 \text{ cm s}^{-1}$ ). In subsequent panels, a set of snapshots zooms in on the spatial domain of Fig. 4a to highlight the different stages of the nonlinear disintegration of the internal tides.





**Figure 3.** Snapshots of the interfacial displacement of leftward-propagating quasi-linear internal tides for run A1 ( $H_1 = 30$  m;  $L_p = 35.49$  km). The amplitude saturation is evident as the tidal forcing is increased and the flow becomes supercritical (see legend). The run time is nine tidal periods.

At a first stage, Fig. 4b, the internal tide splits up into two different groups of rank-ordered solitons: a train of depressions on the leading edge, and a train of elevations, after the former packet, with initially smaller amplitudes. At a later stage, Fig. 4c, the largest elevations have reached the smaller depressions in the train, and three leading solitons at the front present almost equal amplitudes. Previous solitary wave packets, already propagating away from the generation area, are shown in Fig. 4d and e and correspond to preceding disintegrated internal tides. The “table-top” soliton observed at the leading edge of every preceding internal tide emerged in all cases from the first of the three solitons described previously in Fig. 4c.

As the leading soliton evolves and reaches its maximum amplitude, it also broadens, as predicted by soliton wave theory (Helfrich and Melville, 2006), in comparison with subsequent solitons of smaller amplitude (Fig. 4d, e). The observed increase in the distance between the “table-top” soliton and subsequent (smaller) solitons also indicates that, as expected from theory, the leading soliton moves (phase speed) faster than solitons in the tail.

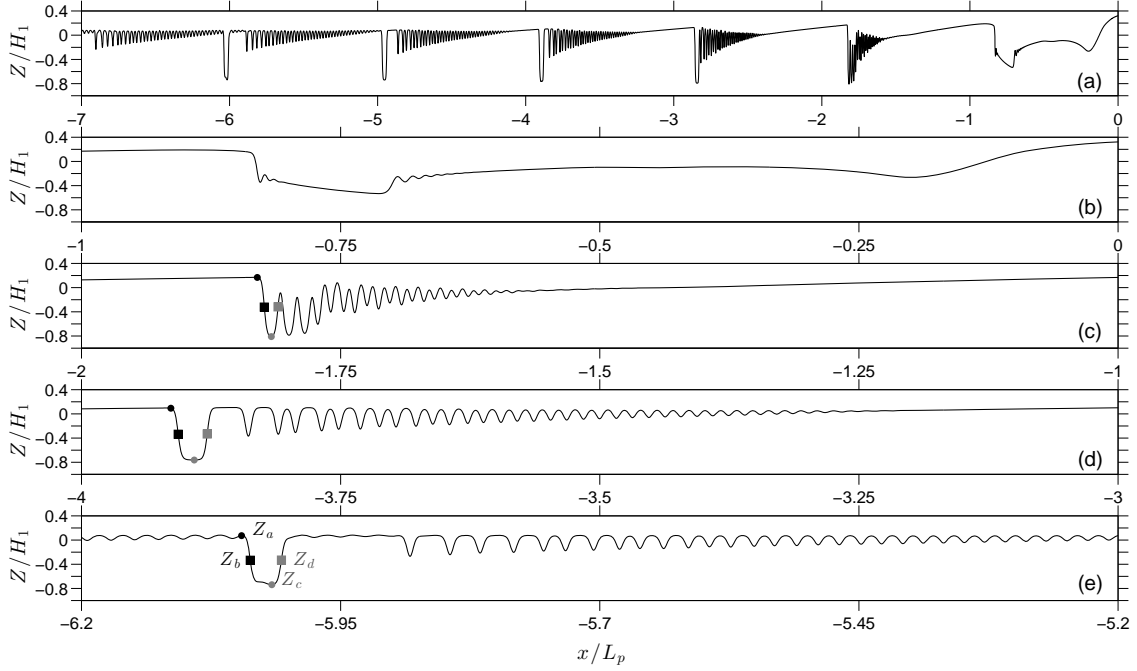
Because tidally generated solitons are part of the evolving internal tides,  $z = 0$  cannot be used as a reference level to compute the amplitude down to the trough of the soliton (see Figs. 1 and 4). Similarly, the soliton width cannot be measured taking  $z = 0$  as a reference level. A criterion is required to adopt a suitable reference level for calculating the soliton amplitude,  $A_s$ , and width,  $L_s$ . Here we introduce the reference level  $Z_a$ , which for every leftward-propagating soliton indicates where the first spatial derivative of the interfacial

displacement,  $Z$ , becomes zero. Accordingly, the soliton amplitude,  $A_s$ , is defined as the vertical distance between  $Z_a$  and the trough of the leading soliton, located at  $Z_b$  (see e.g. in Fig. 4c–e). The soliton width,  $L_s$ , is defined as the horizontal distance between  $Z_c$  and  $Z_d$ , located halfway of the vertical distance spanning  $A_s$  (see also e.g. in Fig. 4c–e). Finally, the soliton phase speed,  $c_s$ , is computed by subtracting the velocity of the (mimicked) tidal flow,  $U$ , from the velocity of the soliton embedded within the internal tide.

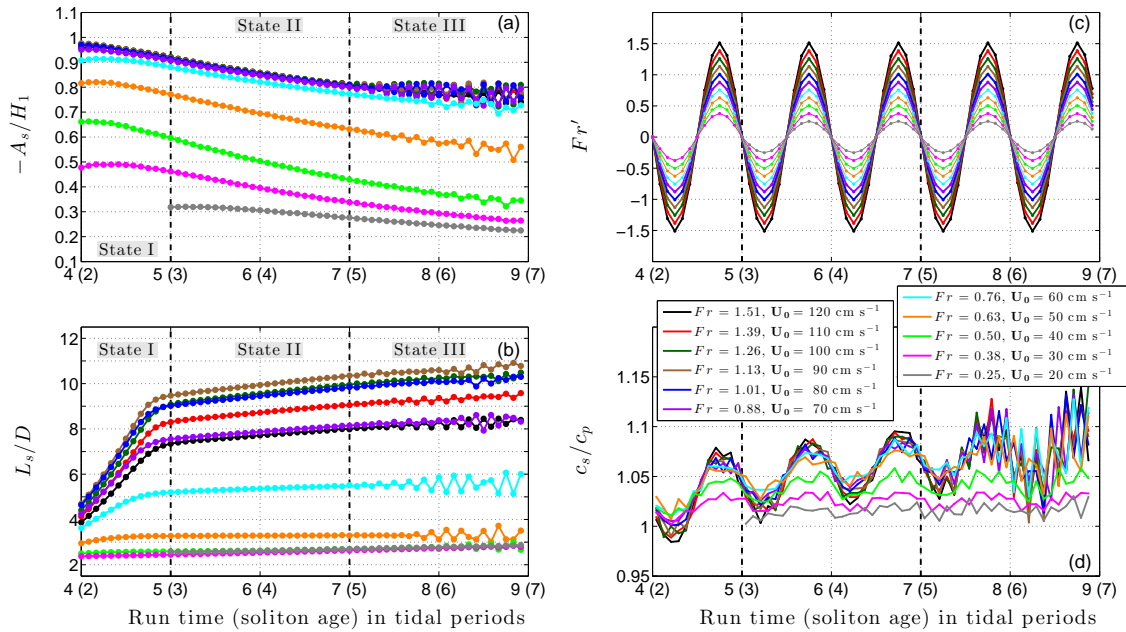
Using the above criteria, Fig. 5 presents the wave evolution of leading solitons under different forcing strengths (see legend) towards a fully developed stage. Contrary to what one might expect, the amplitudes of the leading solitons decrease during their evolution (Fig. 5a). This can be ascribed to their tide-generated nature. At an early stage, the disintegration of the internal tide leads at its front to a large depression, and this subsequently evolves into a mature leading soliton propagating through the tail of the preceding internal tide (see Fig. 4c–e).

The soliton reaches its maximum amplitude slightly before the flow becomes critical ( $Fr = 0.88$ ) and attains the “table-top” form in the supercritical regime when forced with a stronger tidal flow ( $Fr = 1.13$ ). Unexpectedly, when the tidal forcing is increased even further, the soliton width starts to decrease while keeping its maximum amplitude (cf. Fig. 5a and b). This feature is unlike classical eKdV and MCC theories, suggesting that limiting factors related to the forcing may be acting.

Generally speaking, we distinguish between two types of solitons regarding their timescales of growth (see Fig. 5a and



**Figure 4.** Snapshots of the interfacial displacement of nonlinear internal tides and solitons in run A1 for a supercritical regime ( $Fr = 1.13$ ,  $U_0 = 90 \text{ cm s}^{-1}$ ). (a) Overview of leftward-propagating internal tides and solitons. (b–e) Set of spatial zooms from (a) showing different stages of the nonlinear disintegration of the internal tides. Points  $Z_a$  (black dot),  $Z_b$  (grey dot),  $Z_c$  (black square) and  $Z_d$  (grey square) are shown to illustrate how the soliton amplitude,  $A_s$ , and width,  $L_s$ , are computed (see the text in Sect. 5.1 for details). The run time is nine tidal periods. For scaling purposes we recall that, for run A1,  $H_1 = 30 \text{ m}$  and  $L_p = 35.49 \text{ km}$ .



**Figure 5.** Wave evolution of leftward-propagating leading solitons in run A1 under different forcing strengths (see legend). In all panels the horizontal axis indicates the run time and soliton age (in brackets) in tidal periods. The (dimensionless) wave properties are (a) soliton amplitude,  $A_s/H_1$ ; (b) soliton width,  $L_s/D$ ; (c) instantaneous Froude number,  $Fr' = U/c_p$ ; and (d) soliton phase speed,  $c_s/c_p$ . Note that we take  $c_p$  to be negative (leftward propagation) for consistency with the physical meaning of the sign in  $Fr'$ . For scaling purposes, we recall that, in run A1,  $H_1 = 30 \text{ m}$ ,  $D = 100 \text{ m}$  and  $c_p = -79 \text{ cm s}^{-1}$ .

b). First, the smaller and narrower solitons, generated in a subcritical regime and which attain a nearly constant shape quickly after their generation ( $Fr \leq 0.5$ ). Second, the larger and broader solitons, generated in nearly critical and supercritical regimes and which evolve over longer timescales ( $Fr \geq 0.88$ ). We distinguish here three different states for strongly nonlinear solitons, which are indicated with vertical dashed lines and labels in Fig. 5a and b. During State I emerging solitons evolve as transient waves which broaden linearly until they reach a fully developed form. Then, in State II, they preserve their shape in time and, occasionally, may overtake the preceding internal tide, which is State III, causing the oscillations observed in the width, amplitude and phase speed in Fig. 5a, b, and d.

In agreement with the above description, the phase speed graphs also reveal a clear distinction between the subcritical and critical/supercritical regimes (Fig. 5d). On the one hand, smaller solitons show a nearly constant phase speed. They were generated with a small or moderate tidal forcing (subcritical flow). On the other hand, larger solitons present an oscillating phase speed which increases over time. They were generated with a relatively strong tidal forcing (critical and supercritical flow). The oscillation is the response to a governing flow where the accelerating and decelerating phases of the soliton are imposed by the direction of the tidal flow. This is seen by comparing the instantaneous Froude number,  $Fr'$ , in Fig. 5c with the soliton phase speed in Fig. 5d. Crucial moments occur when  $Fr' = -1$  and  $Fr' < -1$ . During the former, solitons cannot propagate against the tidal flow, and remain stationary. During the latter, leftward-propagating solitons experience a rightward advection driven by the larger tidal flow.

Finally, we compare in Fig. 6 the wave properties of mature forced-MCC solitons<sup>3</sup> with KdV-type and MCC soliton solutions (Kakutani and Yamasaki, 1978; Ostrovsky and Stepanyants, 1989; Miyata, 1985, 1988; Choi and Camassa, 1999; Helfrich and Melville, 2006; Gerkema and Zimmerman, 2008). To this aim, the soliton width for KdV-type and MCC theories is computed following the same procedure as for the forced-MCC solitons; that is, we use points  $Z_c$  and  $Z_d$  (see Fig. 4c–e).

As expected, small tide-generated solitons approach the linear long-wave phase speed for interfacial waves ( $c_s/c_p \approx 1$ ), while larger tide-generated solitons have a higher phase speed following a curve as in eKdV and MCC theory. However, because tide-generated solitons ride on internal tides, their wave properties are not simply the response to a two-fluid layer system as such, as happens for eKdV and MCC solitons, but they are also subjected to the forcing of the system and to a variable background flow (the internal tide). We suggest that the above scenario may account for the slower phase speeds of the forced-MCC solitons when compared to

their eKdV and MCC counterparts. Interestingly, this difference slightly decreases as the solitons grow (cf. the length of the coloured dashed lines in Fig. 6a).

As regards the relationship between the soliton width and amplitude, tide-generated solitons follow a similar behaviour to that predicted by eKdV and MCC theory, broadening as they approach their maximum amplitude. By this broadening, strongly nonlinear solitons develop the “table-top” shape, although forced-MCC equations generate some larger and narrower solitons than their eKdV and MCC counterparts (Fig. 6b).

## 5.2 Growth limitation of tide-generated solitons: runs B1 and C1

We use for runs B1 and C1 a similar range of Froude numbers as for run A1; however, they present a more weakly nonlinear regime where a striking feature emerges. Leading solitons exhibit a maximum amplitude which is not related to a “table-top” form and which cannot be exceeded by further increasing the tidal forcing (see Figs. 7a and 8a). They reach this limiting amplitude in both cases when the flow is supercritical (run B1:  $Fr = 1.26$ ; and run C1:  $Fr = 1.33$ ). More importantly, above this limit, the strengthening of the tidal forcing leads to a narrowing and amplitude decrease in the leading solitons (Figs. 7a, b and 8a, b). We recall here that the decrease in the soliton width after reaching its maximum is also observed when the tidal forcing leading to limiting solitons in run A1 is increased (see Fig. 5a, b).

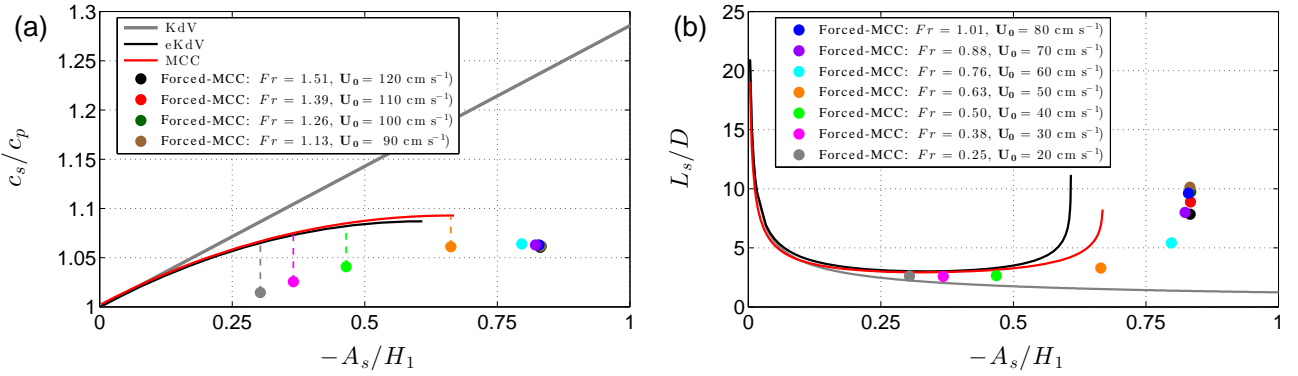
The above results support the idea that tidally generated solitons might be subject to a limited growth which is beyond the classical KdV and MCC-type models, being due to the saturation of the underlying quasi-linear internal tide as the tidal forcing increases (see Sect. 4).

According to their phase speed, and in agreement with findings from run A1, two types of leading solitons also emerge in runs B1 and C1. The larger nonlinear solitons (critical and supercritical regimes) exhibit an oscillating speed, in phase with the tidal flow, which increases over time. The smaller nonlinear solitons (subcritical regime) exhibit a nearly constant phase speed (Figs. 7a, c, d and 8a, c, d).

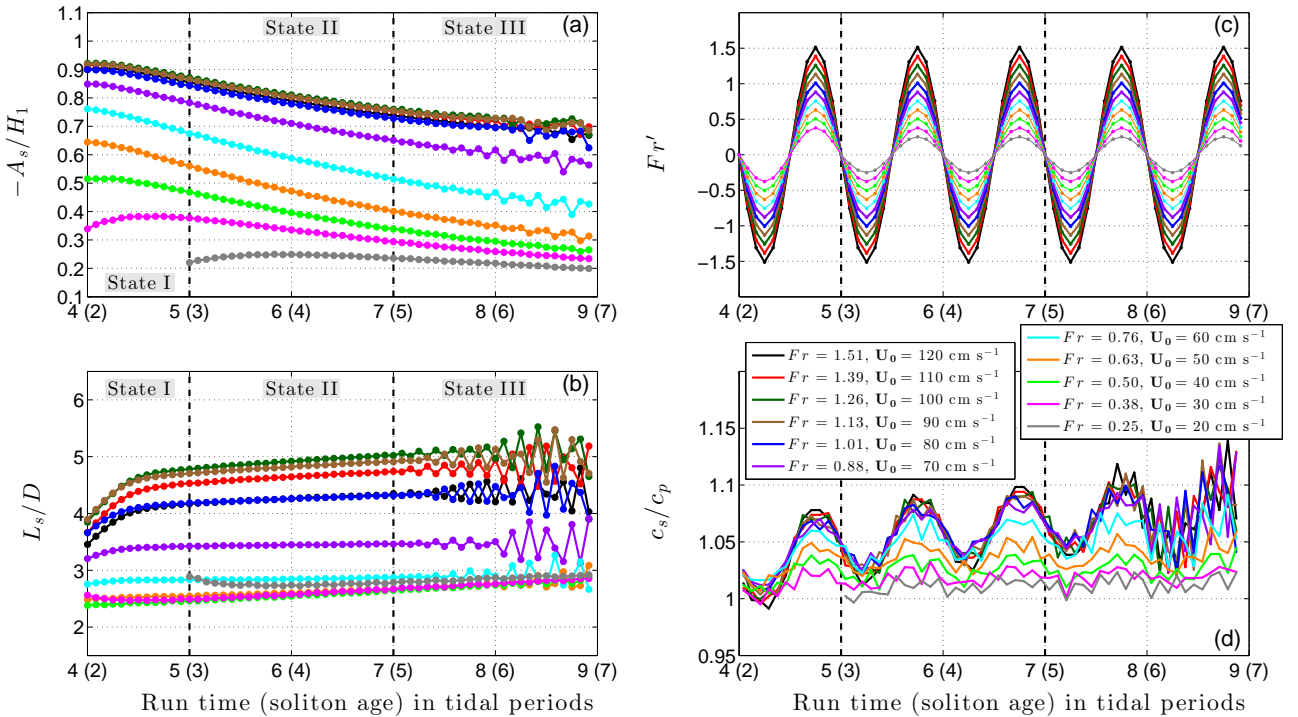
From Figs. 9 and 10, we gain further insight into the different stages by which internal tides generate saturated leading solitons in runs B1 ( $Fr = 1.26$ ,  $U_0 = 100 \text{ cm s}^{-1}$ ) and C1 ( $Fr = 1.33$ ,  $U_0 = 100 \text{ cm s}^{-1}$ ). In contrast to run A1 (Fig. 4), here the internal tides do not split up into two different groups of solitons, but disintegrate into solitary wave packets of rank-ordered depressions. Also, the “table-top” solitary waves that lead the internal tides in run A1 (Fig. 4d, e) are not present in runs B1 and C1, as previously discussed from the wave property analyses. We attribute this absence to the lower height of the topography in run B1 and the decrease in the upper layer thickness in run C1.

On the one hand, the smaller topography generates quasi-linear internal tides which are smaller than those in run A1

<sup>3</sup>These wave properties correspond to solitons of State II (mature solitons) after time averaging over a tidal cycle.



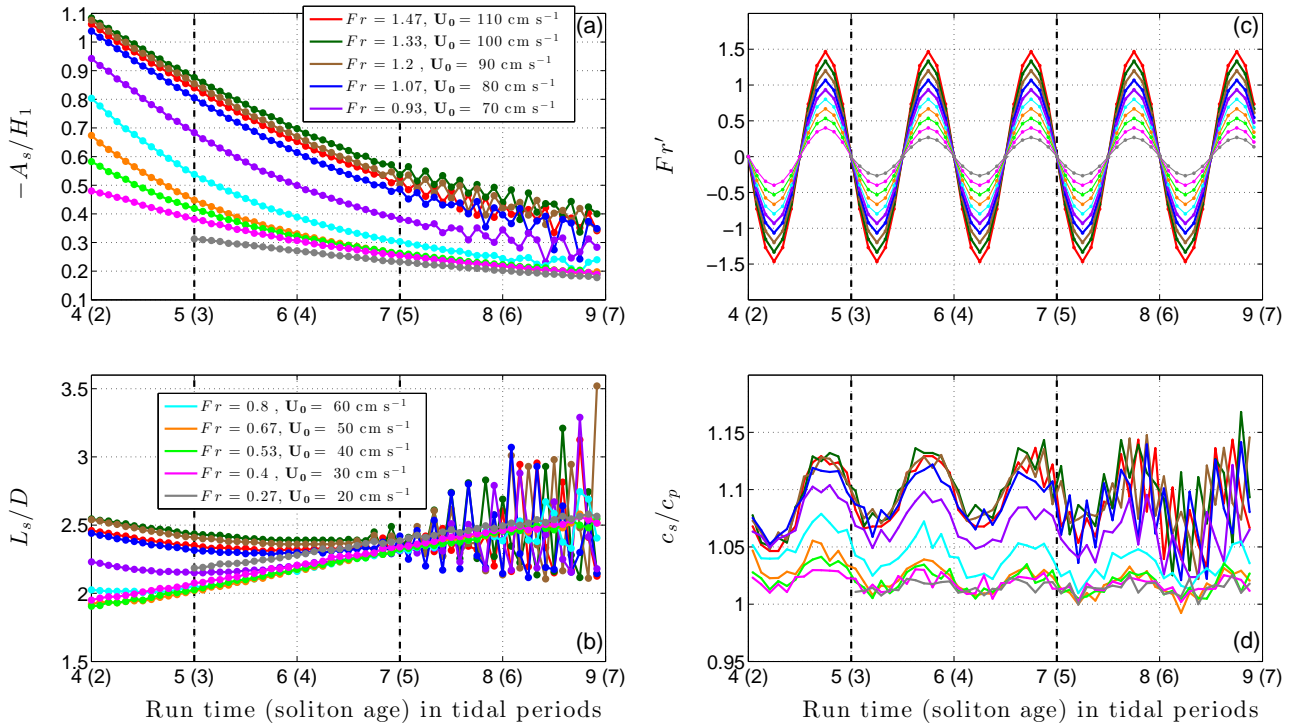
**Figure 6.** Solitary wave solutions for mature leading solitons in run A1 from the KdV (grey line), eKdV (black line) and MCC (red line) theories compared to numerical solutions from the forced-MCC equations (coloured dots refer to the Froude number and strength of the tidal flow; see legend). **(a)** Soliton phase speed scaled to the linear long-wave phase speed for interfacial waves ( $c_s/c_p$ ) vs. soliton amplitude scaled to the thickness of the upper layer ( $-A_s/H_1$ ). **(b)** Soliton width scaled to the total water depth ( $L_s/D$ ) vs. soliton amplitude scaled to the thickness of the upper layer ( $-A_s/H_1$ ).



**Figure 7.** Wave evolution of leftward-propagating leading solitons in run B1 under different forcing strengths (see legend). In all panels the  $x$  axis indicates the run time and soliton age (in brackets) in tidal periods. The (dimensionless) wave properties are **(a)** soliton amplitude,  $A_s/H_1$ ; **(b)** soliton width,  $L_s/D$ ; **(c)** instantaneous Froude number,  $Fr' = U/c_p$ ; and **(d)** soliton phase speed,  $c_s/c_p$ . Note that we take  $c_p$  to be negative (leftward propagation) for consistency with the physical meaning of the different sign in  $Fr'$ . For scaling purposes, we recall that in run B1,  $H_1 = 30$  m,  $D = 100$  m and  $c_p = -79$  cm s $^{-1}$ .

(see Fig. 2). With all other parameters being the same, the smaller internal tide in run B1 then exhibits a weaker nonlinear disintegration. On the other hand, the thinner  $H_1$  in run C1 requires a maximum amplitude to attain the “table-top” form, which is larger than for runs A1 and B1 (see  $-A_m/H_1$  in Table 1). In this context, the smaller quasi-

linear internal tides generated in run C1, by comparison with run A1 (see Fig. 2c), do not lead to strongly nonlinear disintegration in the full forced-MCC model, not even in the supercritical regime of  $Fr > 1$ . Indeed, although both run A1 and run C1 generate leading solitons with a relatively similar amplitude, the latter run exhibits mature leading solitons



**Figure 8.** Same as Fig. 7 but for run C1. For scaling purposes, we recall that, in run C1,  $H_1 = 25$ ,  $D = 100$  and  $c_p = -75 \text{ cm s}^{-1}$ .

which are significantly smaller and narrower (cf. Figs. 4d, e and 10d, e), suggesting that dispersive effects might overcome nonlinearities more noticeably when the upper layer is thinner.

When compared with solitary wave solutions from eKdV and MCC theories, the growth-limiting effect of the tidal forcing becomes a remarkable feature of forced-MCC solitons generated in runs B1 and C1, since they reach a limiting amplitude but do not attain a “table-top” form (Fig. 11b, d). In this context it is also worthwhile noting that in run B1 saturated solitons have amplitudes larger than those predicted by eKdV and MCC theories, whereas in run C1 saturated solitons have amplitudes well below those predicted by eKdV and MCC theories. Counterintuitively, it is also evident from both runs B1 and C1 that the leading solitons have smaller amplitudes and widths as the tidal forcing increases above the saturation point, as previously noted from Figs. 7 and 8.

Regarding the relationship between the soliton phase speed and amplitude, both runs B1 and C1 follow a similar curve to that predicted by the eKdV and MCC theories (Fig. 11a, c), although the phase speed of forced-MCC solutions is slower in all cases, as occurred for run A1 (see Fig. 6a). Also similar to run A1, the deviation in phase speed between MCC and forced-MCC solutions is observed to decrease as the solitons grow (cf. the length of the coloured dashed lines in Fig. 11a, c), suggesting that small solitons might be more subject to forcing effects.

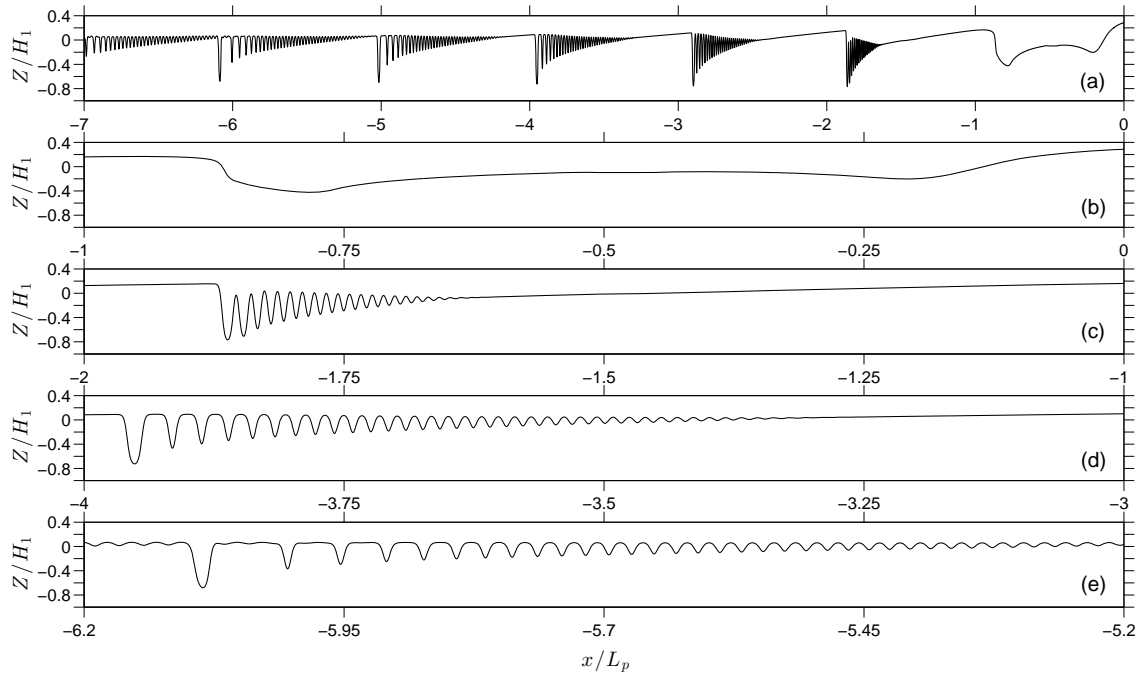
### 5.3 Effects of the Earth’s rotation: runs A1, B1 and C1

In Fig. 12 the effects of the Earth’s rotation on the wave evolution of fully nonlinear tide-generated solitons are shown for runs A1, B1 and C1. The different coloured lines refer to the rotationless case (black line);  $\theta = 15^\circ$ ,  $\mu_p = 0.27$  (green line);  $\theta = 30^\circ$ ,  $\mu_p = 0.52$  (blue line); and  $\theta = 45^\circ$ ,  $\mu_p = 0.73$  (red line).

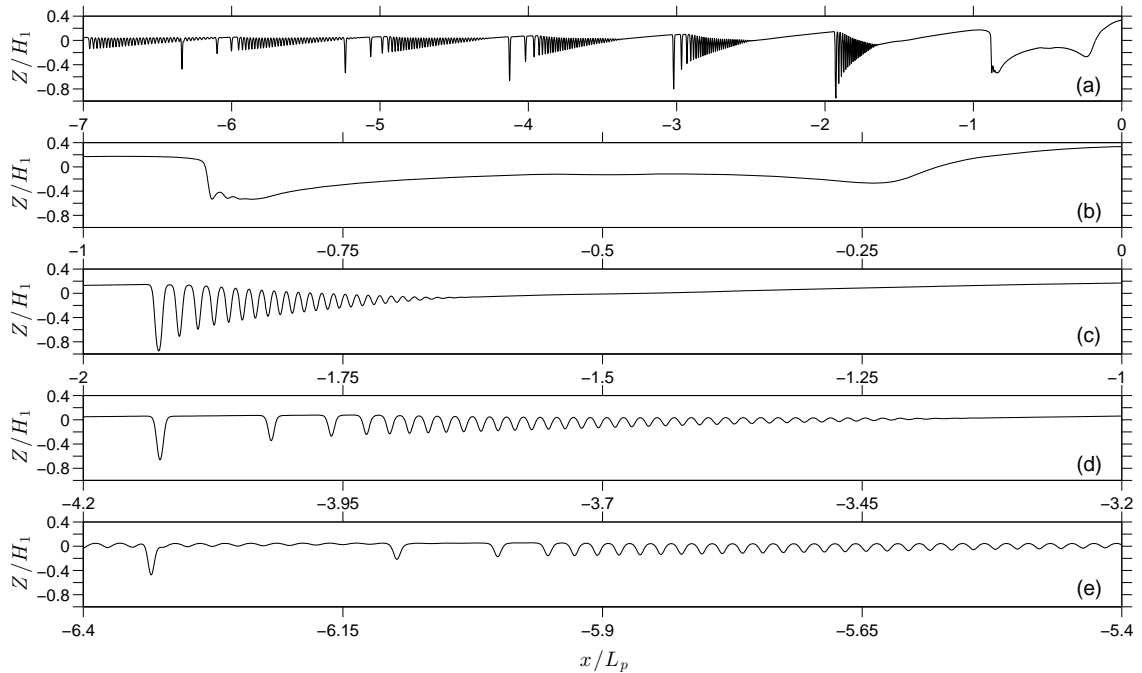
In agreement with previous studies, we observe in all panels that an increase in the latitude leads to larger dispersive effects due to Coriolis dispersion, which prevents the nonlinear internal tide from disintegrating into strongly nonlinear solitons (Gerkema and Zimmerman, 1995; Gerkema, 1996). This causes the long internal waves to envelop less solitary waves. Also, the internal tides are shown to travel faster as rotation becomes stronger, as rotation increases the phase speed of the linear internal tide,  $c_f$  ( $c_f^2 = c_0^2 + f^2/k^2$ , with  $k$  being the wavelength of the internal tide). Although the soliton speeds themselves are only very weakly affected by rotation, they appear to be travelling faster since they are embedded in the internal tide from which they emerge. As a consequence, leading solitons overtake more quickly preceding internal tides.

## 6 Discussion and conclusions

We investigate limiting amplitudes of internal tides and solitons using a generalization of the fully nonlinear MCC equa-

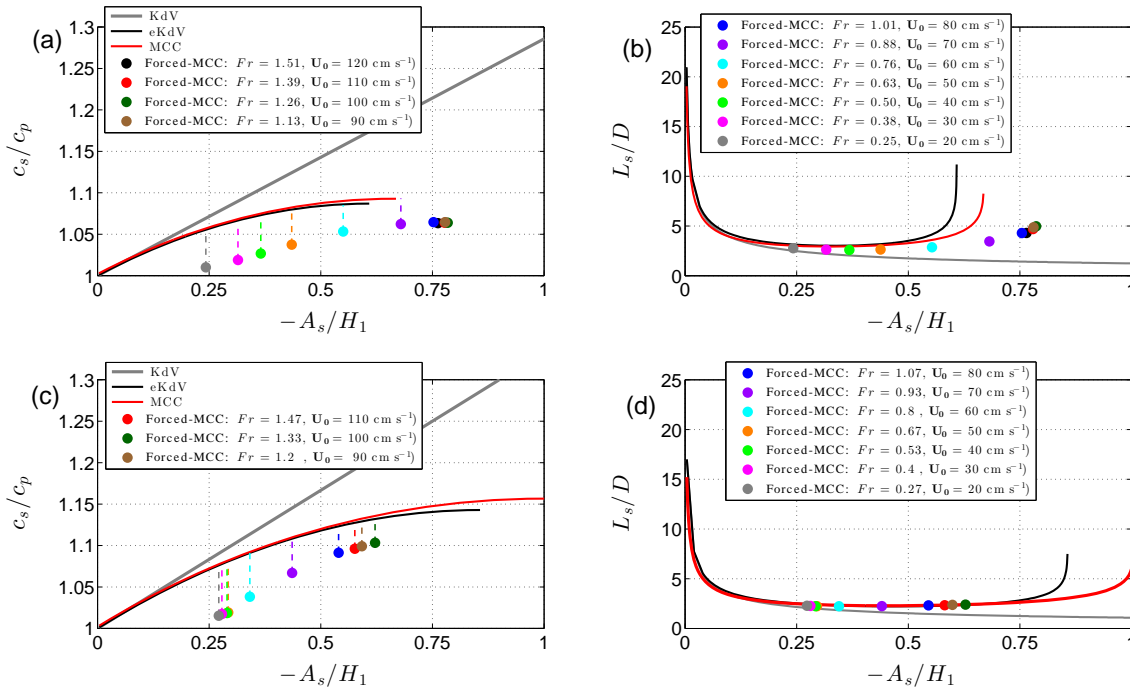


**Figure 9.** Snapshots of the interfacial displacement of nonlinear internal tides and solitons in run B1 for a supercritical regime ( $Fr = 1.26$ ,  $U_0 = 100 \text{ cm s}^{-1}$ ). (a) Overview of leftward-propagating internal tides and solitons. (b–e) Set of spatial zooms from (a) showing different stages of the nonlinear disintegration of the internal tides. The run time is nine tidal periods. For scaling purposes, we recall that, for run B1,  $H_1 = 30 \text{ m}$  and  $L_p = 35.49 \text{ km}$ .

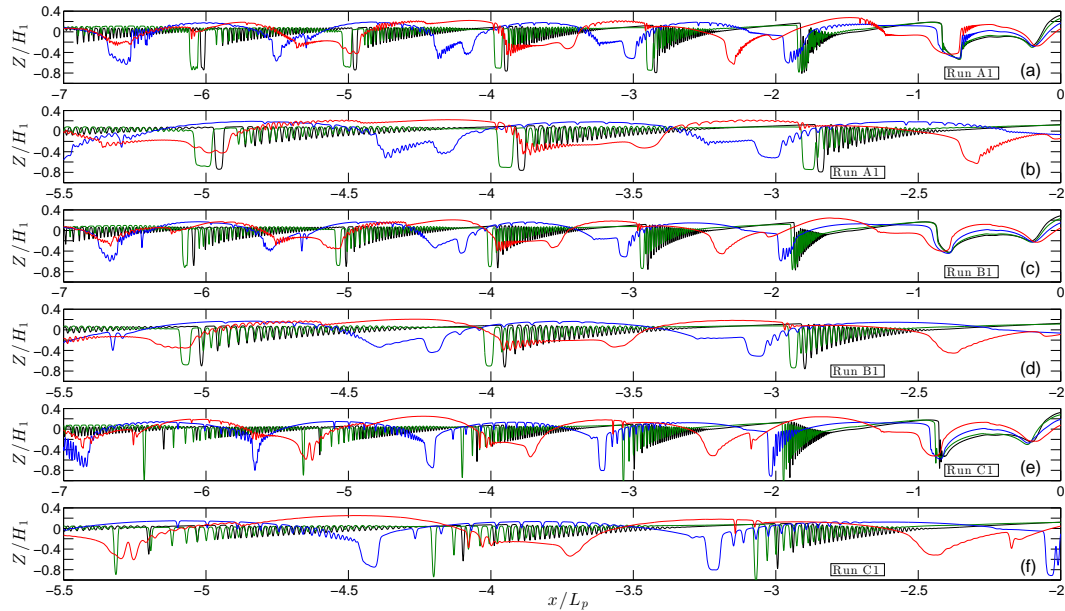


**Figure 10.** Snapshots of the interfacial displacement of nonlinear internal tides and solitons in run C1 for a supercritical regime ( $Fr = 1.33$ ,  $U_0 = 100 \text{ cm s}^{-1}$ ). (a) Overview of leftward-propagating internal tides and solitons. (b–e) Set of spatial zooms from (a) showing different stages of the nonlinear disintegration of the internal tides. The run time is nine tidal periods. For scaling purposes, we recall that, for run C1,  $H_1 = 25 \text{ m}$  and  $L_p = 33.54 \text{ km}$ .





**Figure 11.** Solitary wave solutions for mature leading solitons in run B1 (top row) and run C1 (bottom row) from KdV (grey line), eKdV (black line) and MCC (red line) theories compared to numerical solutions from the forced-MCC equations (coloured dots refer to the Froude number and strength of the tidal flow; see legend). **(a, c)** Soliton phase speed scaled to the linear long-wave phase speed for interfacial waves ( $c_s/c_p$ ) vs. soliton amplitude scaled to the thickness of the upper layer ( $-A_s/H_1$ ). **(b, d)** Soliton width scaled to the total water depth ( $L_s/D$ ) vs. soliton amplitude scaled to the thickness of the upper layer ( $-A_s/H_1$ ).



**Figure 12.** Effects of the Earth's rotation through a set of snapshots from runs A1 ( $Fr=1.13$ ;  $U_0=90\text{ cm s}^{-1}$ ), B1 ( $Fr=1.26$ ;  $U_0=100\text{ cm s}^{-1}$ ) and C1 ( $Fr=1.33$ ;  $U_0=100\text{ cm s}^{-1}$ ). The run time is nine tidal periods. **(a, c, e)** Overview of leftward-propagating tide-generated internal tides and solitons. **(b, d, f)** Spatial zoom from the corresponding overview. In all panels the rotationless case ( $\theta=0$ ,  $\mu_p=0$ ) is shown as a black line. Rotating cases are  $\theta=15^\circ$ ,  $\mu_p=0.27$  (green line);  $\theta=30^\circ$ ,  $\mu_p=0.52$  (blue line); and  $\theta=45^\circ$ ,  $\mu_p=0.73$  (red line).

tions (Miyata, 1985, 1988; Choi and Camassa, 1999), extended here with forcing terms and Coriolis effects (forced-MCC- $f$ ). The focus is on the effects of the forcing, which represents a novelty in the existing literature and provides a closer view to an ocean-like scenario. The mechanism for internal tide generation is represented by a horizontally oscillating sill, mimicking a barotropic tidal flow over topography. Solitons are generated by a disintegration of the internal tide.

The application of an oscillating topography is not completely equivalent to the oceanic case of a tidal flow over a topography at rest. For this reason we have restricted our analyses to a parameter space where a semi-equivalence between both forcing systems was demonstrated (Appendix C). This agreement encourages us to conclude that our findings are not an artifact caused by the use of a mimicked barotropic tidal flow. Of course the findings presented here cannot describe the whole variety of the specific oceanic conditions. However, we believe that this study improves our understanding of the generation and evolution of tide-generated solitons.

Numerical solutions show that strongly nonlinear tide-generated solitons attain in some cases a limiting table-shaped form, in agreement with classical soliton theory. However, results also suggest that tide-generated solitons may alternatively be limited by saturation of the underlying quasi-linear internal tide. In the purely linear system the amplitude of the internal tide increases linearly with the strength of the barotropic tidal flow. But in the quasi-linear case, as the forcing becomes stronger, advective terms become stronger too and cannot be neglected. (Again, in the quasi-linear case, barotropic advection is retained, but interactions of the baroclinic field with itself are neglected). As a result, a saturation in the amplitude of the internal tide occurs; a further increase in the tidal flow does not produce a larger internal tide. This effect seems to have passed unnoticed in previous studies, but might be a key factor in the subsequent disintegration of the internal tide into solitons. It implies that when one includes the genuinely nonlinear effects, i.e. products of baroclinic terms, resulting solitons may stay well below their formal limiting amplitude, no matter how strong the forcing. Interestingly, an increase in the tidal forcing above the value that generates table-shaped solitons, or above the value that *simply* generates solitons attaining an earlier limitation in growth, causes a narrowing and, subsequently, a decrease in amplitude. The upshot is that increasing the tidal forcing above a certain strength does not lead to larger solitons, but, counterintuitively, to smaller ones.

Motivated by the above finding, we performed analogous runs using the full set of weakly nonlinear equations derived in Gerkema (1996). Because these equations are built around the framework of the classical KdV theory and Klein–Gordon equations, one would not expect that an amplitude saturation of solitons could occur. Nevertheless, results (not shown here) demonstrate that both the quasi-linear internal tides and weakly nonlinear tide-generated solitons also ex-

hibit a limiting amplitude. Noting that this model works with an actual tidal flow over a topography at rest, it seems reasonable to argue that the limiting factor is inherent to the tidal forcing. This supports the idea that the forced-MCC- $f$  equations represent an insightful tool for the fully nonlinear framework, where tidally generated solitons may attain limiting amplitudes with or without reaching a table-shaped form.

Another departure from classical theories is that strongly nonlinear tide-generated solitons may exhibit larger maximum amplitudes than predicted from eKdV and MCC solutions, while soliton phase speeds are always smaller. We attribute these differences to the fact that tide-generated solitons *ride* on internal tides and, hence, their wave properties are not simply the response to a two-fluid layer system as such, as in eKdV and MCC solitons, but are also subjected to the forcing of the system, to a variable background flow, and to interfacial displacements of the internal tide itself. In this context, numerical results also show that solitons propagate *freely* from the source only when the tidal flow is small (subcritical flow), while an increase in the tidal forcing (critical and supercritical flow) generates accelerating and decelerating phases of the soliton speed.

In relation to the rotational cases, and in agreement with previous studies (Gerkema and Zimmerman, 1995; Gerkema, 1996), numerical results from the forced-MCC- $f$  equations show that when rotation becomes stronger, the dispersive effect of the Coriolis force becomes stronger too and overcomes nonlinearities, thus preventing the internal tide from disintegrating into solitons.

Before concluding we must note, reiterating arguments by Ostrovsky and Grue (2003), that fully nonlinear, weakly nonhydrostatic models entail a paradox to the effect that strongly nonlinear solitons appear from a set of equations that have strong nonlinearity but weak dispersion, while the very existence of solitons presumes a balance between the two. In our case, the MCC-type model is used, involving only the lowest-order nonhydrostatic dispersive terms. Despite the small parameter featuring in the nonhydrostatic terms, they may actually become large in practice (i.e. in the numerical runs) if internal wave profiles are steepening, hence contradicting the original assumption. Indeed, there is no guarantee that the higher-order dispersive terms, which were dropped from these equations, would always remain small. A suggestion for future work is, therefore, to check our results against a numerical computation with a fully nonlinear nonhydrostatic set of equations.

## 7 Data availability

The modeling data used by this study are freely available but not otherwise published in any publicly accessible database. The data can nonetheless be provided on request via e-mail to the first author.



## Appendix A: Numerical strategy

We define a grid in time and space for discretization of the various derivatives of the system. Then,

$$t_n = n \Delta t \quad \text{and} \quad x_j = j \Delta x$$

are introduced for integer values of  $n$  (time step) and  $j$  (spatial step), where  $\Delta t$  and  $\Delta x$  are the magnitude of the steps. Time- and spatial-dependent variables are described as e.g.  $y(t_n, x_j)$ , at any time and position. Thus,  $y_j^n$  is the value of the variable  $y$  at the current time and spatial step,  $n$  and  $j$ , respectively. Consequently,  $n+1$  represents the “next time step”, and so  $n-1$  is the “previous time step”, and analogously for  $j$  in the spatial grid.

The various derivatives in the model are discretized with centered difference approximations (Durrán, 1999) as follows:

$$y_t(t_n, x_j) \cong \frac{y_j^{n+1} - y_j^n}{\Delta t}, \quad (\text{A1})$$

$$y_x(t_n, x_j) \cong \frac{y_{j+1}^n - y_{j-1}^n}{2\Delta x}, \quad (\text{A2})$$

$$y_{xx}(t_n, x_j) \cong \frac{y_{j+1}^n - 2y_j^n + y_{j-1}^n}{(\Delta x)^2}, \quad (\text{A3})$$

$$y_{xt}(t_n, x_j) \cong \frac{y_{j+1}^{n+1} - y_{j+1}^n - (y_{j-1}^{n+1} - y_{j-1}^n)}{2\Delta x \Delta t}, \quad (\text{A4})$$

$$y_{xxt}(t_n, x_j) \cong \frac{y_{j+1}^{n+1} - y_{j+1}^n - 2(y_j^{n+1} - y_j^n) + (y_{j-1}^{n+1} - y_{j-1}^n)}{(\Delta x)^2 \Delta t}. \quad (\text{A5})$$

Initially the system is at rest with horizontal velocities,  $\bar{u}_i$  and  $\bar{v}_i$ , and displacement of the interface,  $\zeta$ , being all zero at the first two time levels ( $n-1, n$ ). The thickness of the upper,  $h_1$ , and lower,  $h_2$ , layers, together with the topography,  $h(X)$ , describes the two-layer system. At the next time step ( $n+1$ ), we start to move the topography to the right, creating the effect of a tidal motion flowing to the left. For given  $U$ , i.e. scaled velocity of moving topography (Eq. 47), and time step, the excursion of the topography is a known quantity which is used to shift (first, second and third) spatial derivatives of  $h(X)$  at every new time step.

The time derivatives of the  $\bar{v}_i$  momentum and continuity equations (51), (52) and (53) are solved numerically using the third-order Adams–Bashforth approximation (Durrán, 1999), for which  $\bar{v}_1$ ,  $\bar{v}_2$  and  $\zeta$  at the next time step ( $n+1$ ), and at all  $j$  positions, are determined in terms of the known quantities at the previous two time steps ( $n-1, n$ ).

However, solving numerically  $\bar{u}_1$  from Eq. (49) is not straightforward, as we deal with three different time derivatives of  $\bar{u}_1$  accompanied by space–time-dependent coefficients. Thus, after collecting the various time derivatives involving  $\bar{u}_1$  on the one side, and all remaining terms on the other side, the horizontal momentum equation of  $\bar{u}_1$  takes an expression of the form

$$a \bar{u}_{1,t} + b \bar{u}_{1,x} + c \bar{u}_{1,xx} = Y(t_n, x_j), \quad (\text{A6})$$

where  $a$ ,  $b$  and  $c$  represent spatial derivatives of space–time-dependent variables ( $\zeta(x, t)$  and  $h(x, t)$ ), and  $Y(t_n, x_j)$  represents a collection of known quantities whose values may be dependent on time and/or space. In the remainder, we describe the numerical method to solve this set of partial differential equations. If we treat the time derivative as a collective term on the left-hand side, we can write

$$(a \bar{u}_{1,t} + b \bar{u}_{1,x} + c \bar{u}_{1,xx})_t = Y(t_n, x_j) + (a_t \bar{u}_1 + b_t \bar{u}_{1,x} + c_t \bar{u}_{1,xx}), \quad (\text{A7})$$

which leads us to the introduction of a new variable,  $\bar{U}_1$ , which groups coefficients  $a$ ,  $b$ , and  $c$  and time derivatives of  $\bar{u}_1$  and turns our problem into a numerically solvable expression of the form

$$\bar{U}_{1,t} = Y(t_n, x_j) + (a_t \bar{u}_1 + b_t \bar{u}_{1,x} + c_t \bar{u}_{1,xx}). \quad (\text{A8})$$

It is important to recall here that  $Y(t_n, x_j)$  and the spatial derivatives of  $\bar{u}_1$  are both evaluated at the current time step ( $n$ ); the time derivatives of  $a$ ,  $b$  and  $c$ , which involve values of  $\zeta$  at the current ( $n$ ) and new time step ( $n+1$ ), have been previously evaluated with Eq. (53) via Adams–Bashforth approximation. This allows us to rewrite the above expression as

$$\bar{U}_{1,t} = R(t_n, x_j) \quad (\text{A9})$$

by grouping all known quantities on the right-hand side under the variable  $R(t_n, x_j)$ . Next we need to discretize the time derivative of  $\bar{U}_1$ , but before doing that, we discretize its spatial derivatives using Eqs. (A2) and (A3), resulting in

$$\begin{aligned} \bar{U}_1 &= \left( a_j - \frac{2c_j}{2\Delta x} \right) \bar{u}_{1j} + \left( \frac{-b_j}{2\Delta x} + \frac{c_j}{(\Delta x)^2} \right) \bar{u}_{1j-1} \\ &+ \left( \frac{b_j}{2\Delta x} - \frac{c_j}{(\Delta x)^2} \right) \bar{u}_{1j+1}, \end{aligned}$$

which we rewrite by introducing factors  $d$ ,  $e$  and  $f$  as follows:

$$\bar{U}_{1j} = d_j \bar{u}_{1j} + e_j \bar{u}_{1j-1} + f_j \bar{u}_{1j+1}. \quad (\text{A10})$$

If we now discretize the time derivative of  $\bar{U}_1$  and apply Adams–Bashforth, we obtain a numerically solvable expression for  $\bar{U}_1$  at the next time step, which reads

$$\bar{U}_{1j}^{n+1} = \bar{U}_{1j}^n + \frac{\Delta t}{12} (23R_j^n - 16R_j^{n-1} + 5R_j^{n-2}), \quad (\text{A11})$$

where  $\bar{U}_{1j}^{n+1}$  actually includes

$$\bar{U}_{1j}^{n+1} = d_j^{n+1} \bar{u}_{1j}^{n+1} + e_j^{n+1} \bar{u}_{1j-1}^{n+1} + f_j^{n+1} \bar{u}_{1j+1}^{n+1}. \quad (\text{A12})$$

To close our system, we still need to obtain  $\bar{u}_{1j}^{n+1}$  for all  $j$  terms. To that end, the equation above is more complicated to solve and gives rise to implicit equations, as we not only

have the unknown  $\bar{u}_{1j}^{n+1}$ , but also  $\bar{u}_{1j-1}^{n+1}$  and  $\bar{u}_{1j+1}^{n+1}$ , which come from the mixed second and third derivatives of  $u_1$  in Eq. (A6). However, this is a well-known problem that can be solved using the tridiagonal matrix algorithm (TDMA), also known as the Thomas algorithm (Logan, 1987).

The choice of the space–time steps  $\Delta t$  and  $\Delta x$  is based on two main requirements. Firstly, the resolution in  $x$  ( $\Delta x$ ) must be sufficiently fine to resolve third-derivative terms and ensure that any short, solitary-like waves are properly resolved. Nevertheless, Kelvin–Helmholtz instabilities may not be filtered out. In this type of model, Jo and Choi (2002) found that solitary waves of sufficient amplitude could be unstable at high wavenumbers due to Kelvin–Helmholtz instability. Thus, if the grid resolution is too fine, unstable short waves will emerge near the wave crest and ultimately explode numerically (Jo and Choi, 2002; Helfrich and Melville, 2006; Helfrich and Grimshaw, 2008). In some cases, the instability can be controlled by filtering out wavenumbers above a threshold (W. Choi, personal communication, 2007; cited in Helfrich and Grimshaw, 2008). For our numerical experiments we consider a  $\Delta x$  course enough to prevent the problem. A second condition follows from the requirement of stability. Thus, for a given spatial step one may take the Courant–Friedrichs–Lewy condition for the linearized equations as an indication of the required time step. The criterion implies that  $\Delta x/\Delta t$  should be larger than the phase speed of the wave, taking special care where the advection by the barotropic tidal flow (here mimicked with the moving topography) should be added to the phase speed to apply the criterion properly (Gerkema, 1994).

For the simulations we present, it was not needed to filter out wavenumbers above a threshold to control Kelvin–Helmholtz instabilities, as we designed the space–time grid to avoid this problem. However, in some cases, especially in the simulations where the forcing was fairly strong, an additional trick was needed to retain stability around the generation area (Gerkema, 1994). In those cases averages were taken in the vicinity of the top of the sill (around the steepest part of the topography), where the instabilities arose. At one particular point  $(x_j, t_n)$  in space–time, new values of  $\bar{u}_i$ ,  $\bar{v}_i$  and  $\zeta$  were calculated by taking the average of the old values at  $x_{j-1}$ ,  $x_j$  and  $x_{j+1}$ , and subsequently in time between  $t_n$  and  $t_{n-1}$ . The disturbance provoked by this procedure was tested and found to be a minor effect only, as it was only applied over the closest region to the top of the topography.

## Appendix B

### B1 Forced-MCC- $f$ model equations

In Appendix A, the numerical scheme used to solve the model is explained using a generic expression (A6) for the  $\bar{u}_i$  horizontal momentum equation (49). Here we present the full set of nondimensional forced equations actually used for

the numerical solving of the model. The procedure is as follows.

Firstly, all terms of the  $\bar{u}_i$  horizontal momentum equation (49) are worked out and grouped according to their physical effects (i.e. linear, nonlinear and dispersive effects from the upper and lower layers, and from topography), leaving unknown quantities involving time derivatives of  $\bar{u}_1$  on the left-hand side. The resulting expression (B1) resembles (A6), where coefficients  $a$ ,  $b$  and  $c$  involve derivatives of space–time-dependent variables and  $Y(t_n, x_j)$  is represented here by the sum of all terms on the right-hand side,

$$\begin{aligned} a \bar{u}_{1,t} &+ b \bar{u}_{1,xt} + c \bar{u}_{1,xtt} = \\ \text{linear} &+ \text{nonlinear} + \text{dispersive}_1 + \text{dispersive}_2 \\ &+ \text{dispersive}_{\text{topo}} + \frac{\delta \eta_2}{(1-h)} \\ &\left[ (\eta_2 h_x - \eta_2 \zeta_x) \phi_x - \frac{\eta_2^2}{3} \phi_{xx} \right. \\ &\left. + \phi \left( \frac{\eta_2}{2} h_{xx} + \zeta_x h_x \right) \right], \end{aligned} \quad (\text{B1})$$

$$\bar{u}_2 = \frac{U h - \eta_1 \bar{u}_1}{\eta_2}, \quad (\text{50})$$

$$\bar{v}_{1,t} = -\mu \bar{u}_1 - \bar{u}_1 \bar{v}_{1,x} + O(\delta^2), \quad (\text{51})$$

$$\bar{v}_{2,t} = -\mu \bar{u}_2 - \bar{u}_2 \bar{v}_{2,x} + O(\delta^2), \quad (\text{52})$$

$$\zeta_t = (h_1 - \zeta) \bar{u}_{1,x} - \bar{u}_1 \zeta_x, \quad (\text{53})$$

with

$$\phi = \frac{1}{\eta_2} \left[ h U_t + U^2 h_x + (\bar{u}_1 - \bar{u}_2) (\eta_1 \bar{u}_{1,x} - \bar{u}_1 \zeta_x) + \bar{u}_2 U h_x \right], \quad (\text{B2})$$

$$\begin{aligned} a(\zeta, h) &= 1 + \frac{\delta \eta_2}{1-h} \left[ (\eta_2 h_x - \eta_2 \zeta_x) (\eta_1 / \eta_2)_x \right. \\ &\left. - \frac{\eta_2^2}{3} (\eta_1 / \eta_2)_{xx} + \frac{\eta_1}{\eta_2} \left( \frac{\eta_2}{2} h_{xx} + \zeta_x h_x \right) \right], \end{aligned} \quad (\text{B3})$$

$$\begin{aligned} b(\zeta, h) &= \delta \left( 1 - \frac{\eta_1}{1-h} \right) \eta_1 \zeta_x \\ &+ \frac{\delta \eta_2}{1-h} \left[ \frac{\eta_1}{\eta_2} (\eta_2 h_x - \eta_2 \zeta_x) \right. \\ &\left. - \frac{2\eta_2^2}{3} (\eta_1 / \eta_2)_x \right], \end{aligned} \quad (\text{B4})$$

$$c(\zeta, h) = -\delta \left( 1 - \frac{\eta_1}{1-h} \right) \frac{\eta_1^2}{3} - \frac{\delta \eta_2}{(1-h)} \frac{\eta_1 \eta_2}{3}, \quad (\text{B5})$$

$$\text{linear} = \mu \bar{v}_1 + \zeta_x + \frac{1}{1-h} \left[ h U_t + U^2 h_x + \bar{u}_2 h_t \right], \quad (\text{B6})$$

$$\begin{aligned} \text{nonlinear} = & -\bar{u}_1 \bar{u}_{1,x} + \frac{1}{1-h} [(\bar{u}_1 - \bar{u}_2) \zeta_t + \bar{u}_1 \eta_1 \bar{u}_{1,x} \\ & + \bar{u}_2 \eta_2 \bar{u}_{2,x} - \mu(\eta_1 \bar{v}_1 + \eta_2 \bar{v}_2) - \eta_1 \zeta_x], \end{aligned} \quad (\text{B7})$$

$$\begin{aligned} \text{dispersive}_1 = & \delta \left( 1 - \frac{\eta_1}{1-h} \right) \\ & \left[ -\eta_1 \zeta_x \left( \bar{u}_1 \bar{u}_{1,xx} - (\bar{u}_{1,x})^2 \right) \right. \\ & \left. + \frac{\eta_1^2}{3} (\bar{u}_1 \bar{u}_{1,xxx} - \bar{u}_{1,x} \bar{u}_{1,xx}) \right], \end{aligned} \quad (\text{B8})$$

$$\begin{aligned} \text{dispersive}_2 = & \frac{\delta \eta_2}{1-h} \left[ -\eta_2 \zeta_x \left( \bar{u}_2 \bar{u}_{2,xx} - (\bar{u}_{2,x})^2 \right) \right. \\ & \left. - \frac{\eta_2^2}{3} (\bar{u}_2 \bar{u}_{2,xxx} - \bar{u}_{2,x} \bar{u}_{2,xx}) \right], \end{aligned} \quad (\text{B9})$$

$$\begin{aligned} \text{dispersive}_{\text{topo}} = & \frac{\delta \eta_2}{(1-h)} \left[ \bar{u}_2 h_x (\eta_2 \bar{u}_{2,xx} + \zeta_x \bar{u}_{2,x}) \right. \\ & + \frac{\eta_2}{2} (U_t h_{xx} + U^2 h_{xxx} + 2U \bar{u}_{2,x} h_{xx} \\ & + 2\bar{u}_2 U h_{xxx} + 3\bar{u}_2 \bar{u}_{2,x} h_{xx} + \bar{u}_2^2 h_{xxx}) \\ & + \zeta_x (U_t h_x + U^2 h_{xx} \\ & \left. + 2\bar{u}_2 U h_{xx} + \bar{u}_2^2 h_{xx}) \right]. \end{aligned} \quad (\text{B10})$$

## B2 Linear and quasi-linear forced-MCC- $f$ model equations

The quasi-linear forced-MCC- $f$  model follows from neglecting the purely nonlinear terms and weakly nonhydrostatic dispersive terms in Eqs. (B1) and (50)–(53). The equations are linear with regard to the baroclinic fields, but the coefficients become time-dependent due to barotropic advection (which is prescribed) and, therefore, higher harmonics will be generated when the forcing is increased. The quasi-linear version of the forced-MCC- $f$  equations reads as

$$\begin{aligned} \bar{u}_{1,t} = & \mu \bar{v}_1 + \zeta_x \\ & + \frac{1}{1-h} \left[ h U_t + U^2 h_x + \bar{u}_2 h_t \right. \\ & \left. - \mu (h_1 \bar{v}_1 + (h_2 - h) \bar{v}_2) - h_1 \zeta_x \right], \end{aligned} \quad (\text{B11})$$

$$\bar{u}_2 = \frac{U h - h_1 \bar{u}_1}{h_2 - h}, \quad (\text{B12})$$

$$\bar{v}_{1,t} = -\mu \bar{u}_1, \quad (\text{B13})$$

$$\bar{v}_{2,t} = -\mu \bar{u}_2, \quad (\text{B14})$$

$$\zeta_t = h_1 \bar{u}_{1,x}. \quad (\text{B15})$$

We notice that the linear runs were actually done somewhat indirectly by taking the quasi-linear version of forced-MCC- $f$  equations above, Eqs. (B11)–(B15), and reducing the forcing by a factor of 100 since the quasi-linear terms cannot be removed explicitly in this model setting without also removing the forcing. Afterwards we enhance the amplitude in the plots accordingly. By reducing the forcing, we effectively enter the linear regime.

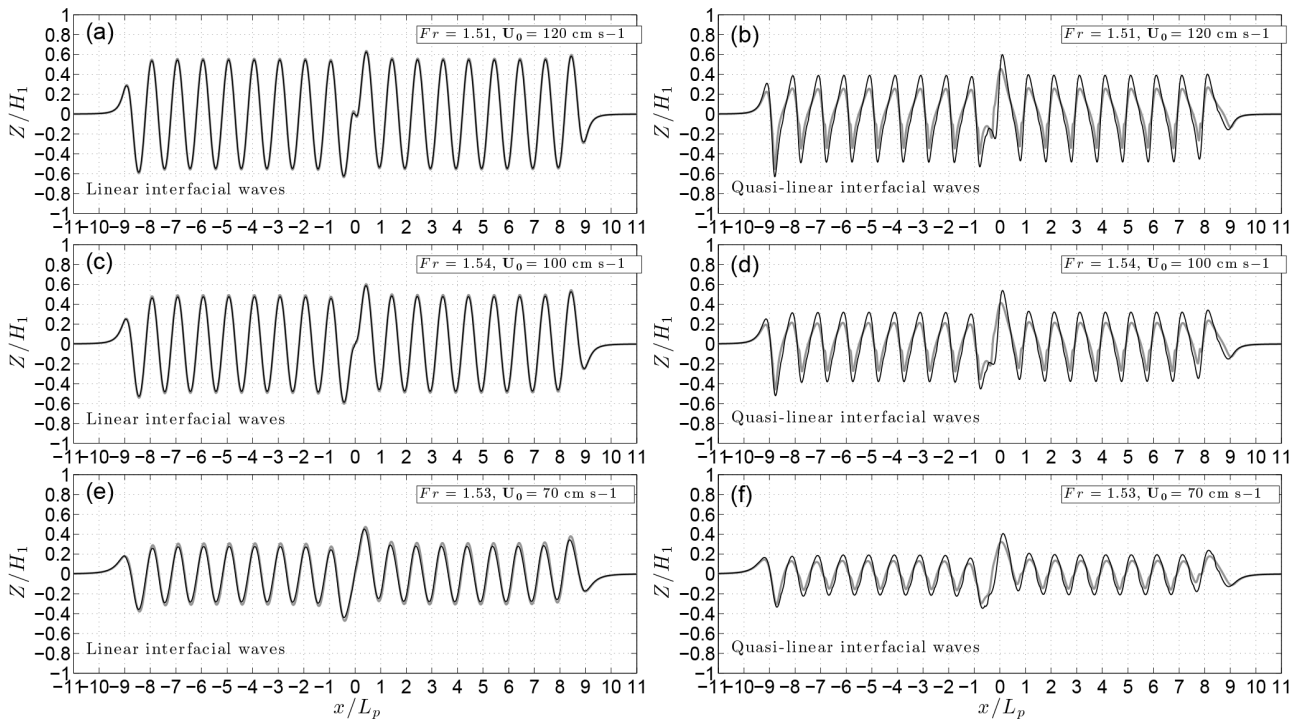
## Appendix C: Oscillating topography vs. tidal flow

A Galilean transformation involves two frames of reference which move with constant and rectilinear speed with respect to each other. Hence, observations made in one frame can be converted to another, as physical laws are identical. However, our oscillating topography is not an inertial frame since it is accelerated with respect to a situation where the topography is at rest (as in the ocean). It is, therefore, not evident that the results from the two frames are equivalent.

We use the generation model of weakly nonlinear, weakly nonhydrostatic interfacial waves derived in Gerkema (1996), which works with tidal motion over a fixed topography, as a benchmark for testing the impact of our “non-inertial” frame of reference. If we compare interfacial waves generated from the nonlinear version of both models, differences are expected to arise from the fact that forced-MCC equations are fully nonlinear. For this reason we restrict the comparison to the linear and quasi-nonlinear model versions. If the results between the forcing systems turn out to be similar, it seems reasonable to assume an equivalence in the nonlinear case as well.

In Appendix Fig. C1, interfacial waves generated from both models are presented for various numerical experiments under a fairly strong forcing, i.e. when both models may be expected to deviate more noticeably from each other. Our interests focus then on the upper limit of the supercritical regime ( $Fr > 1$ ) that we can reach while still preserving a good agreement between both generation mechanisms. The different settings in Fig. C1 differ in the strength of stratification from top to bottom panels, while the thicknesses of the upper and lower layers ( $H_1 = 30$  m,  $H_2 = 70$  m) and the height and width of the sill are kept fixed ( $H_T = 40$  m and  $H_L = 10$  km in Eq. 54).

Results from Fig. C1 indicate that in all cases a close correspondence exists between numerical solutions from Gerkema (1996) (grey line) and the forced-MCC equations (black line), suggesting only a minor impact of the non-inertial nature of our frame of reference when reaching up to  $Fr \sim 1.5$ . These results encourage us to interpret the speed of the oscillating topography as the “strength of the tidal flow” within the parameter space of this study.



**Figure C1.** Linear (left panels) and quasi-linear (right panels) interfacial waves generated via a tidal flow over a sill from the model equations derived in Gerkema (1996) (grey line) and via a horizontally oscillating sill from the model equations derived in this study (black line). The Froude number and corresponding strength of the (mimicked) tidal flow are indicated in the upper-right corner of each panel. For scaling purposes one must note that the wavelength of the linear long-wave interfacial wave,  $L_p$ , varies from top to bottom panels as  $L_p = 35.5$  km ( $g' = 0.03$  m s $^{-1}$ ) in (a) and (b);  $L_p = 29$  km ( $g' = 0.02$  m s $^{-1}$ ) in (c) and (d); and  $L_p = 20.5$  km ( $g' = 0.01$  m s $^{-1}$ ) in (e) and (f). The run time is nine tidal periods.

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